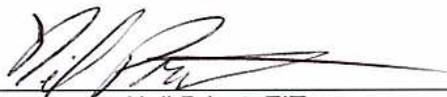


**Red River Community Centre  
Proposed Playground and Skatepark  
Geotechnical Investigation and Evaluation  
FINAL REPORT  
February 2010**

**Prepared By**



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Neil Privat, EIT.  
Geotechnical Designer

**Approved By**



---

Mark Jamieson, P.Eng.  
Senior Geotechnical Engineer





February 8, 2010

File No. 09-0109-04

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Scatliff + Miller + Murray  
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Winnipeg, Manitoba  
R3B 0P4

ATTENTION: Ms. Jennifer Wagner

RE: Red River Community Centre  
Proposed Playground and Skatepark  
Geotechnical Investigation and Evaluation  
Final Report

---

Dear Ms. Wagner:

KGS Group is pleased to submit our final report summarizing the geotechnical investigation and evaluation of the proposed playground and skatepark at the Red River Community Centre.

Included in the final report are the site plan and summary soil logs completed as part of the investigation.

We thank you for the opportunity to provide geotechnical engineering services for this project. Please call the undersigned if you have any questions on the enclosed.

Yours truly,

A handwritten signature in black ink, appearing to read 'Mark Jamieson', written over a light green rectangular background.

Mark Jamieson, P.Eng.  
Senior Geotechnical Engineer

NCP/jr  
Enclosure

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## 1.0 INTRODUCTION

KGS Group was authorized by Scatliff + Miller + Murray Inc. to undertake a geotechnical investigation and evaluation, as well as a topographic survey, of the proposed playground and skate park development at the Red River Community Centre. This report provides a summary of the field investigation results performed to date, as well as geotechnical considerations that should be incorporated into the design of the proposed works.

The geotechnical engineering services provided for this project are outlined below:

- **Geotechnical Investigation** – A subsurface drilling investigation program consisting of power auger drilling at the proposed playground and skate park area to determine the subsurface stratigraphy and foundation conditions. Representative soil samples were collected for material identification and laboratory testing.
- **Topographic Survey** – A topographic survey of existing facilities, trees/vegetation and existing ground elevations.
- **Laboratory Testing** – Diagnostic laboratory index testing on select soil samples to identify engineering soil properties relevant to the assessment.
- **Geotechnical Evaluation** – A geotechnical engineering evaluation of the site conditions at the proposed skate park for consideration in the design.
- **Summary Report** – A comprehensive report outlining the work conducted, laboratory test results and geotechnical considerations for incorporation into the proposed design and construction.

## **2.0 BACKGROUND**

The development of a playground and skate park has been proposed for the northeast corner of the Red River Community Centre on Main Street between Murray and Ridgecrest Avenues in Winnipeg, Manitoba, as shown on Figure 1. The site is currently a green space, but was previously the location of the Red River School and parking lot. The site was leveled with fill as part of the demolition of the school, and turn into soccer fields. In general, the proposed playground will be located within and around the footprint of the removed school. The skate park will be located west of the demolished school, close to Main Street. The travel surface and features of the skate park will generally consist of cast-in-place concrete.

The existing community centre and parking lot to the south and west of the proposed skate park (see Figure 1) was recently constructed (2006). An investigation by M. Block and Associates Ltd. conducted in 2004 titled "Geotechnical Investigation for the Proposed Red River Community Centre Redevelopment Project", reported the drilling of six test holes within the footprints of the community centre building and parking lot. In addition, the report made recommendations for pile, slab on grade and pavement designs.

### **3.0 INVESTIGATION PROGRAM**

#### ***Site Survey***

A topographic site survey was performed by KGS Group in August 2009 to determine ground elevations and locate the existing infrastructure and trees on the site. The existing site conditions and proposed works overlaid on an air photo background are included on Figure 1. This information was provided electronically to Scatliff+Miller+Murray separately.

#### ***Drilling Program***

A drilling and sampling program consisting of eight test holes was completed on August 5, 2009, with drilling services performed by Paddock Drilling Ltd. of Brandon, Manitoba, with on-site supervision and sampling by KGS Group. The locations of the test holes are shown on Figure 1. The test holes were completed using a truck mounted Canterra 250 drill rig, equipped with 125 mm diameter solid stem augers. Soil samples were recovered from the auger flights, with all soils visually inspected in the field for material type and classification according to the Unified Soil Classification System (USCS). Detailed test hole logs incorporating field observations and subsequent laboratory test data are included in Appendix A.

#### ***Laboratory Testing***

Laboratory testing was performed on select soil samples to determine the relevant engineering properties of the subsurface soils. The laboratory testing was completed by National Testing Laboratories Ltd., and included 46 moisture content analyses and 2 Atterberg Limits tests. The results of the testing are shown on the summary logs in Appendix A.

#### ***Stratigraphy***

In general, the stratigraphy at the site has been interpreted by KGS Group to consist of topsoil/clay fill at surface over high plasticity silty clay with a silt layer, occurring within the upper few metres from ground surface, and silt till at depth.

Topsoil was encountered in 2 test holes, with clay fill observed in the other 6 test holes; the topsoil and clay fill supported grass vegetation. The topsoil was of high plasticity and contained organic matter. The clay fill typically contained trace sand and gravel and was of high plasticity. The thickness of both materials was typically less than 0.5 m from ground level. The topsoil and fill was underlain by a deposit of high plasticity silty clay of glaciolacustrine origin. The upper portion of the silty clay was generally stiff and moist, and contained a trace of organic matter. The silty clay was typically soft to firm in consistency with depth, and moist. From the M. Block and Associates Ltd. report, the silty clay extended to an approximate depth of 17.5 m below ground where it was underlain by silt till. The silt layer within the silty clay varied in depth from 1.5 to 2.3 m below ground surface, and was typically moist, soft, of low plasticity and up to 1.5 m in thickness. Minor groundwater infiltration from the silt was observed in 5 of the 8 test holes.

Two key considerations of the encountered soils relative to the skatepark and playground development include:

- The silt layer may be susceptible to frost action / heave and ice lensing.
- The high plasticity silty clay is typically compressible, and susceptible to swelling and shrinking with changes to moisture content.

## **4.0 DESIGN CONSIDERATIONS**

This section is intended to identify general geotechnical considerations for incorporation into the design and construction of the proposed playground and skateboard park. The final design of the proposed works should be reviewed by a qualified geotechnical engineer familiar with the local soil conditions and behavior to ensure that the geotechnical considerations relative to structure performance are effectively incorporated into the design.

### **4.1 GEOTECHNICAL**

#### ***Structural Design***

Although the details of the design have not been finalized, it is understood by KGS that the proposed playground and skate park will include several concrete features and travel surfaces including stairs and ramps at different levels. If the structures are supported on shallow foundations, which is typical for other skate parks in Winnipeg, there will be variable loading applied to the foundation soil. This variable loading may induce differential settlements, potentially causing cracking of the cast-in-place concrete with resulting movements that could affect the serviceability of the proposed works. Structural design of the features to allow for this potential cracking at preferred locations is prudent to minimize their potential impacts on the structure performance and serviceability.

#### ***Subgrade Preparation***

Preparation of the subgrade is necessary to provide a suitable and stable surface for the various structures. The subgrade preparation should include excavation to intact mineral soil, and disposal of topsoil and organic-rich material. The stripped surface should then be compacted to a minimum of 95% of the Standard Proctor Maximum Dry Density (SPMDD). The typical depth of stripping is estimated to be approximately 0.5 m, based on the test hole drill results. Where additional unsuitable subgrade material is encountered (e.g. wet silt, soft clay, organic material, etc.), additional sub-excavation to a minimum depth of 0.6 m should be performed and backfilled with compacted granular fill.

To further improve foundation conditions, a layer of woven geotextile could be placed overtop of the stripped and compacted subgrade. This will help distribute the applied load more uniformly, and bridge over any potential weaker zones. Installation should follow manufacturer's guidelines, with care to protect against tears, folds or wrinkles in the fabric.

The silt layer found across the site will typically be susceptible to frost action, potentially causing heaving and ice lensing during winter below the structures. Typical local practice is to excavate and replace the silt with crushed rockfill, while providing improved subsurface drainage. However, it is likely impractical and cost prohibitive to remove all the silt material, given the observed depth and thickness. An alternative to excavation and replacement would be to reduce the risk of frost penetration into the silt below the concrete structures. This could be achieved by either building up the ground surface around and below the skate park to increase the depth of burial, or by placement of a rigid thermal insulation to reduce the depth of frost penetration. If insulation is used, it would have to be designed for the overlying structure loading.

The foundation preparation below the concrete features should include placement and compaction of at least 600 mm of granular sub-base material. The sub-base should be placed in lifts not exceeding 150 mm compacted. The sub-base material should consist of durable, free draining sand and gravel. All granular material used as sub-base should be compacted to a minimum of 98% SPMDD.

### ***Subsurface Drainage Control***

Changes to the moisture content of the silty clay foundation soil can lead to shrinkage (drying) or swelling (wetting), which could affect the performance of the structures. Construction practices used in the design of the skate park should include methods to control subsurface drainage, and in particular excessive water that could lead to swelling. This will also reduce excess free water that could be available for ice lensing during winter. The following measures should be incorporated into the design to help control the subsurface drainage:

- The excavated subgrade should be positively sloped to promote runoff and minimize ponding below the structures.

- A granular sub-drainage system should be installed below the structures, consisting of a free draining granular fill. To improve subsurface water collection perforated drains could be installed within the granular fill or within excavated trenches.
- The drainage system should be sloped such that all collected water can be removed from the site. The water can be drained either into the municipal drainage system, or to a sump for pump discharge.

## 4.2 CONCRETE

The concrete travel surface and skate features of the skate park should be constructed with control joints and articulation at locations that could tolerate minor movements. This will reduce the risk of potential cracking of the cast-in-place concrete at undesirable locations. All concrete should be designed in accordance with CSA A23.1 and A23.2.

## 5.0 CONCLUSIONS

The stratigraphy at the site consisted of topsoil and clay fill overlying high plasticity silty clay and silt till. A silt layer was encountered within the upper few metres of ground surface, from which water infiltration was observed entering some test holes. This stratigraphy could pose some general concerns related to shallow foundation support for the proposed skate park structures, primarily related to swelling of the silty clay and frost heave / ice lensing associated with the wet silt layer.

The design and construction of the proposed skate park should include features to minimize the risk of adverse movement causing unacceptable performance of the structures associated with the geotechnical conditions at the site. This includes subgrade preparation, placement and compaction of granular fill over the prepared subgrade, and control of subsurface drainage underneath the skate park and playground structures. In addition, measures to minimize the risk of frost action should be considered, including placement of insulation or additional fill to limit frost penetration into the silt layer.

## **6.0 STATEMENT OF LIMITATIONS AND CONDITIONS**

### ***Third Party Use of Report***

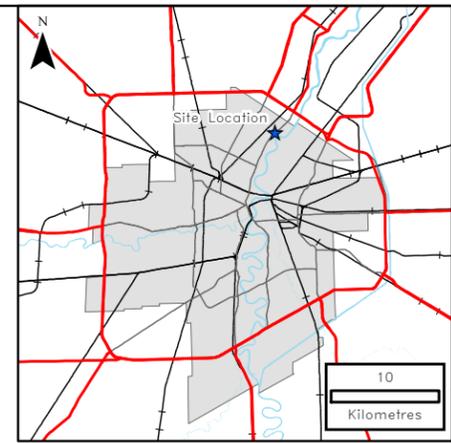
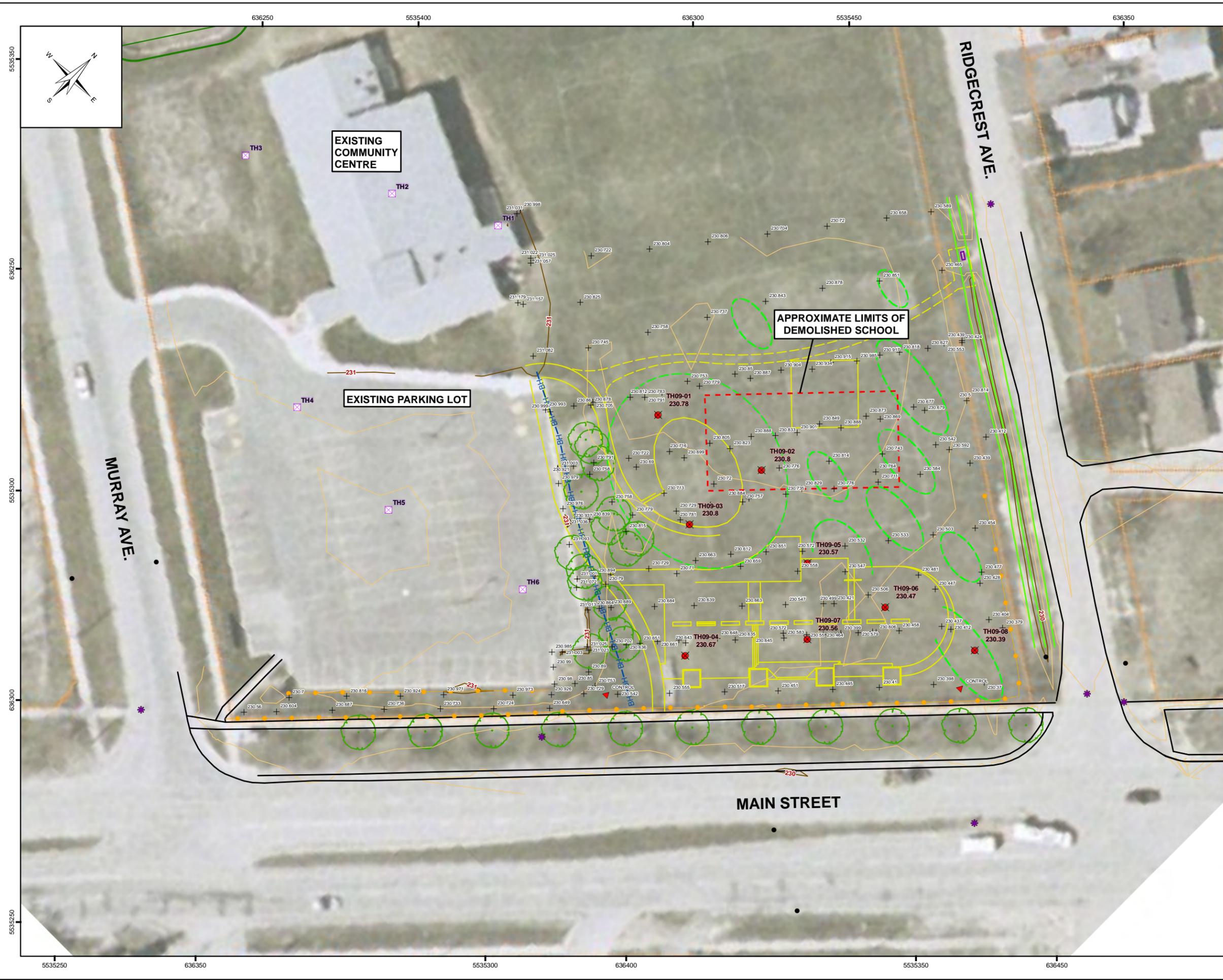
This report has been prepared for Skatliff + Miller + Murray Inc. and any use a third party make of this report, or any reliance on or decisions made based on it, are the responsibility of such third parties. KGS Group accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions undertaken based on this report.

### ***Statement of Limitations***

The geotechnical investigation findings and recommendations of this report were prepared in accordance with generally accepted professional engineering principles and practice. The findings and recommendations are based on the results of field and laboratory investigations, combined with an interpolation of soil and groundwater conditions found at and within the depth of the test holes drilled by KGS at this site. If conditions encountered during construction appear to be different from those shown by the test holes drilled by KGS or if the assumptions stated herein are not in keeping with the design, this office should be notified in order that the recommendations can be reviewed and modified if necessary.

KGS Group makes no representation concerning the legal significance of its finding or the value of the property investigated.

**FIGURE**



**LEGEND:**

- CATCH BASIN
- ✱ MANHOLE
- ✱ TH09-01 TEST HOLE (KGS GROUP, 2009)
- ✱ TH1 TEST HOLE (M. BLOCK, 2004)
- ▲ SURVEY CONTROL POINT (TEMPORARY)
- x GROUND ELEVATION (m)
- FENCE LINE
- BH-BH BURIED HYDRO LINE
- DITCH
- MAILBOX
- 1 m INDEX CONTOUR
- 0.25 m CONTOUR
- PROPOSED CONTOUR
- PROPOSED CONCRETE
- TREE, EXISTING

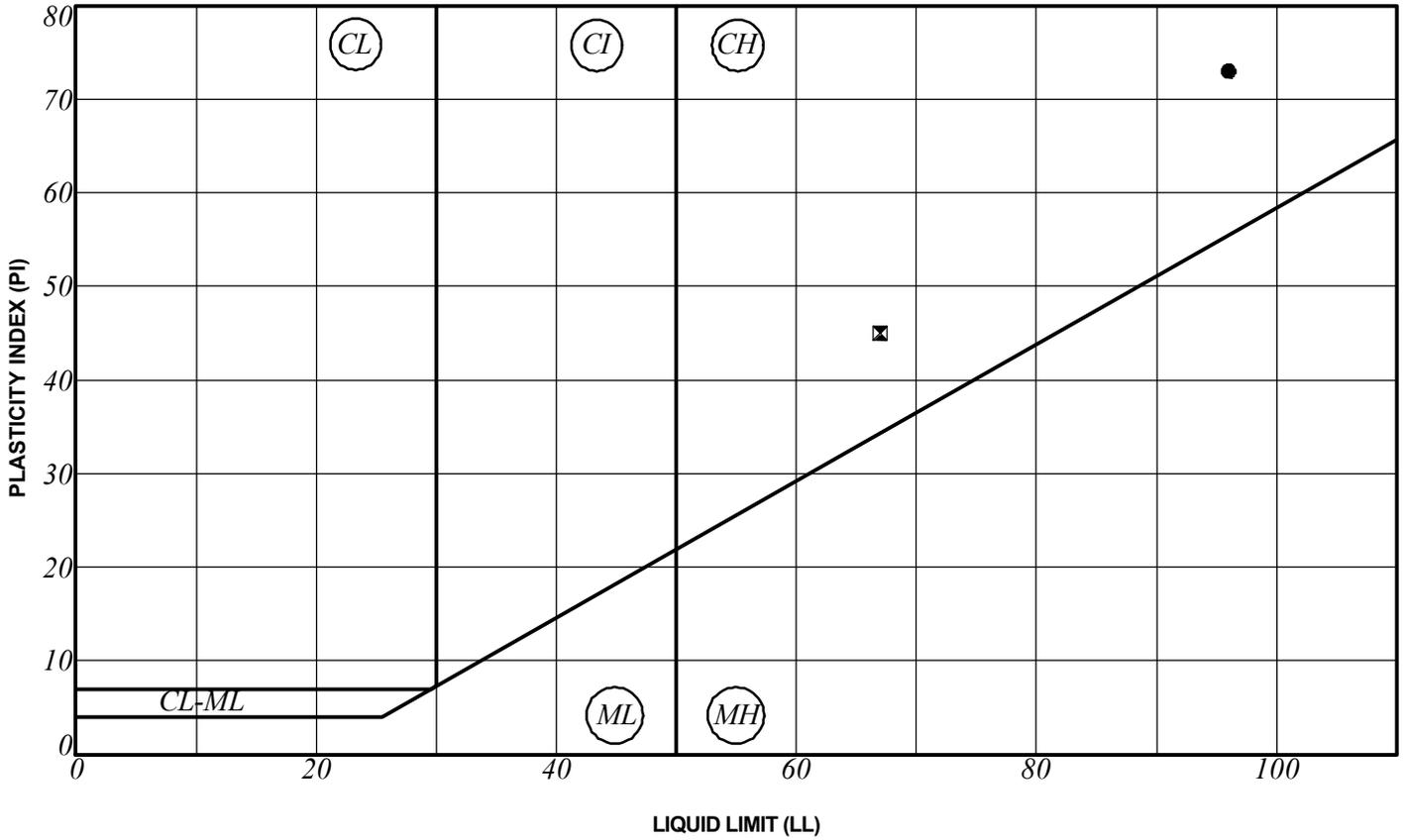
10 0 10 20  
Metres  
SCALE: 1:600 METRIC 11"x17"

- NOTES:**
1. ALL UNITS ARE METRIC AND IN METRES UNLESS OTHERWISE SPECIFIED.
  2. TRANSVERSE MERCATOR PROJECTION, NAD 1983, ZONE 14, CSRS. ELEVATIONS ARE IN METRES ABOVE SEA LEVEL (MSL), (CGVD 28).
  3. SURVEY COMPLETED BY KGS GROUP AUG 07/2009.
  4. AIRPHOTO SUPPLIED BY SCATLIFF + MILLER + MURRAY.
  5. PROPOSED SKATE PARK OUTLINE PROVIDED BY SCATLIFF + MILLER + MURRAY.

A	10/02/09	ISSUED WITH FINAL REPORT	MRJ
NO.	YY/MM/DD	DESCRIPTION	BY
REVISIONS / ISSUE			
<b>KGS GROUP</b>		<b>SCATLIFF+MILLER+MURRAY</b>	
CONSULTING ENGINEERS			
RED RIVER COMMUNITY CENTRE PROPOSED SKATE PARK DEVELOPMENT SITE PLAN			
FEBRUARY 2010		FIGURE 01	0

## APPENDICES

**APPENDIX A**  
**TEST HOLE LOGS**



SYMBOL	HOLE	DEPTH (m)	SAMPLE #	LL	PL	PI	% SAND	% SILT	% CLAY	% MC	CLASSIFICATION
●	TH09-05	1.2		96	23	73				33.9	CH
⊠	TH09-05	4.7		67	22	45				42.4	CH

- Notes:**
- ML - Low Plasticity Silt
  - MH - High Plasticity Silt
  - CL-ML - Silty Clay
  - CL - Low Plasticity Clay
  - CI - Intermediate Plasticity Clay
  - CH - High Plasticity Clay
  - LL - Liquid Limit
  - PL - Plastic Limit
  - PI - Plasticity Index
  - MC - Moisture Content
  - NP - Non-Plastic

<b>KGS GROUP</b>	<b>SCATLIFF+MILLER+MURRAY</b>
Red River Community Centre Proposed Skate Park Development	
<b>A-LINE PLOT</b>	
Feb 2010	Figure A
Page 1 of 1	

**CLIENT** SCATLIFF+MILLER+MURRAY  
**PROJECT** Red River Community Centre Proposed Skate Park Development  
**SITE** NE corner of Main St. & Ridgecrest Ave.  
**LOCATION** 58 m South of Ridgecrest Ave., 58 m West of Main St. (See Figure 1)  
**DRILLING METHOD** 125 mm ø Solid Stem Auger, CT 250 Canterra

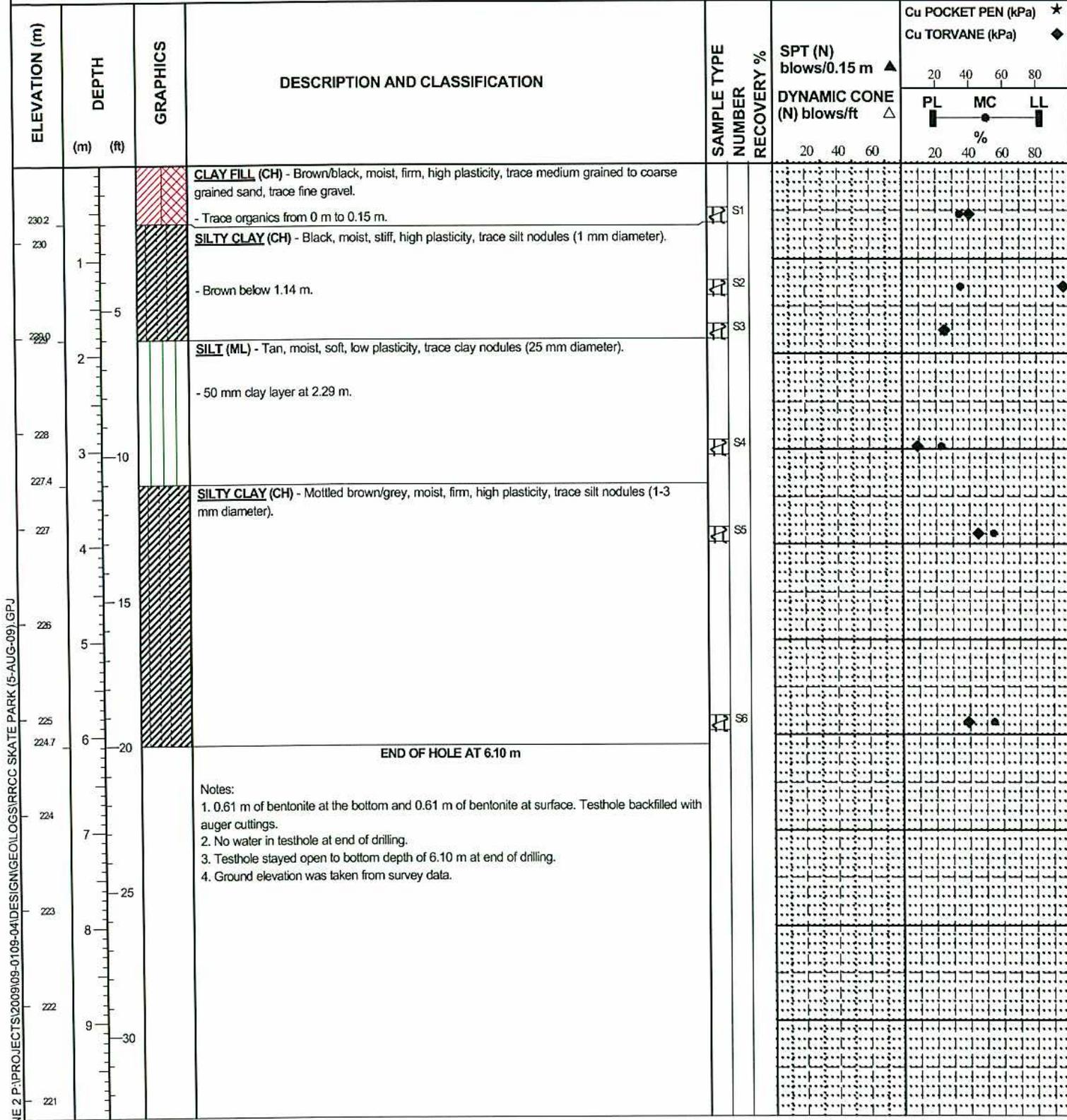
**JOB NO.** 09-0109-04  
**GROUND ELEV.** 230.8 m  
**TOP OF PVC ELEV.**  
**WATER ELEV.**  
**DATE DRILLED** 8/5/2009  
**UTM (m)** N 5,535,380  
 E 636,340

ELEVATION (m)	DEPTH (m) (ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE NUMBER	RECOVERY %	SPT (N) blows/0.15 m ▲	DYNAMIC CONE (N) blows/ft △	Cu POCKET PEN (kPa) ★			Cu TORVANE (kPa) ◆		
								PL	MC	LL			
230.3	0		<b>TOPSOIL</b> - Black, moist, firm, high plasticity, trace rootlets. - Trace silt from 0 m to 0.30 m.	S1									
230	0.5		<b>SILTY CLAY (CH)</b> - Brownish grey, moist, stiff, high plasticity. - Trace silt lenses (3 mm diameter) below 1.52 m.	S2									
229	1			S3									
228.6	2		<b>SILT (ML)</b> - Tan, moist, soft, low plasticity. - Water infiltration below 2.29 m.  - 50 mm clay layer at 2.74 m. - Trace clay below 3.05 m. - Increased moisture content between 3.05 m and 3.35 m.	S4									
228	2.5			S5									
227.1	3		<b>SILTY CLAY (CH)</b> - Grey, moist, firm, high plasticity.  - Trace silt nodules below 4.42 m.	S6									
227	3.5			S7									
226	4												
225	5												
224.7	6		<b>END OF HOLE AT 6.10 m</b>										
224	6.5		Notes: 1. 0.61 m of bentonite at the bottom and 0.61 m bentonite at surface. Testhole backfilled with auger cuttings. 2. Testhole collapsed at 2.44 m below ground surface. 3. Ground elevation was taken from survey data.										
223	7												
222	8												
221	9												

SPT & TORVANE 2 P:IPROJECTS\2009\09-0109-04\DESIGN\GEOLOGS\RRCC SKATE PARK (5-AUG-09)\GPJ

**CLIENT** SCATLIFF+MILLER+MURRAY  
**PROJECT** Red River Community Centre Proposed Skate Park Development  
**SITE** NE corner of Main St. & Ridgcrest Ave.  
**LOCATION** 43 m South of Ridgcrest Ave., 41 m West of Main St. (See Figure 1)  
**DRILLING METHOD** 125 mm ø Solid Stem Auger, CT 250 Canterra

**JOB NO.** 09-0109-04  
**GROUND ELEV.** 230.8 m  
**TOP OF PVC ELEV.**  
**WATER ELEV.**  
**DATE DRILLED** 8/5/2009  
**UTM (m)** N 5,535,392  
 E 636,359



SPT & TORVANE 2 P:\PROJECTS\2009\09-0109-04\DESIGN\GEOLOGS\RRCC SKATE PARK (5-AUG-09).GPJ

**CLIENT** SCATLIFF+MILLER+MURRAY  
**PROJECT** Red River Community Centre Proposed Skate Park Development  
**SITE** NE corner of Main St. & Ridgcrest Ave.  
**LOCATION** 57 m South of Ridgcrest Ave., 30 m West of Main St. (See Figure 1)  
**DRILLING METHOD** 125 mm ø Solid Stem Auger, CT 250 Canterra

**JOB NO.** 09-0109-04  
**GROUND ELEV.** 230.8 m  
**TOP OF PVC ELEV.**  
**WATER ELEV.**  
**DATE DRILLED** 8/5/2009  
**UTM (m)** N 5,535,373  
 E 636,356

ELEVATION (m)	DEPTH (m) (ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE NUMBER	RECOVERY %	SPT (N) blows/0.15 m ▲	DYNAMIC CONE (N) blows/ft △	Cu POCKET PEN (kPa) ★			Cu TORVANE (kPa) ◆						
								20	40	60	80	PL	MC	LL	20	40	60
230.3			<b>TOPSOIL</b> - Black, moist, firm, crumbly, high plasticity, trace fine to coarse grained sand.	S1													
230	1		<b>SILTY CLAY (CH)</b> - Brown, moist, stiff, high plasticity, trace silt nodules (1 - 5 mm diameter).	S2													
229	5																
228.8	2		<b>SILT (ML)</b> - Tan, moist, soft, low plasticity.	S3													
228			- Firm, trace clay below 2.74 m.														
227.6	3		<b>SILTY CLAY (CH)</b> - Mottled brown/grey, moist, firm, high plasticity, trace silt nodules (1-5 mm diameter).	S4													
227	4																
226	15																
225	5																
224.7	6		<b>END OF HOLE AT 6.10 m</b>	S5													
224	7		Notes: 1. 0.61 m of bentonite at the bottom, 0.61 m of bentonite at surface. Testhole backfilled with auger cuttings. 2. Water level measured at 5.49 m below ground at end of drilling. 3. Testhole stayed open to bottom depth of 6.10 m at end of drilling. 4. Ground elevation was taken from survey data.														
223	25																
222	9																
221	30																

SPT & TORVANE 2 P:\PROJECTS\2009\09-0109-04\DESIGN\GEO\LOGS\RRCC SKATE PARK (5-AUG-09).GPJ

SAMPLE TYPE Auger Grab

CONTRACTOR  
**Paddock Drilling Ltd.**

INSPECTOR  
**O. Wang**

APPROVED MRTJ DATE 2/8/10

**CLIENT** SCATLIFF+MILLER+MURRAY  
**PROJECT** Red River Community Centre Proposed Skate Park Development  
**SITE** NE corner of Main St. & Ridgecrest Ave.  
**LOCATION** 61 m South of Ridgecrest Ave., 11 m West of Main St. (See Figure 1)  
**DRILLING METHOD** 125 mm ø Solid Stem Auger, CT 250 Canterra

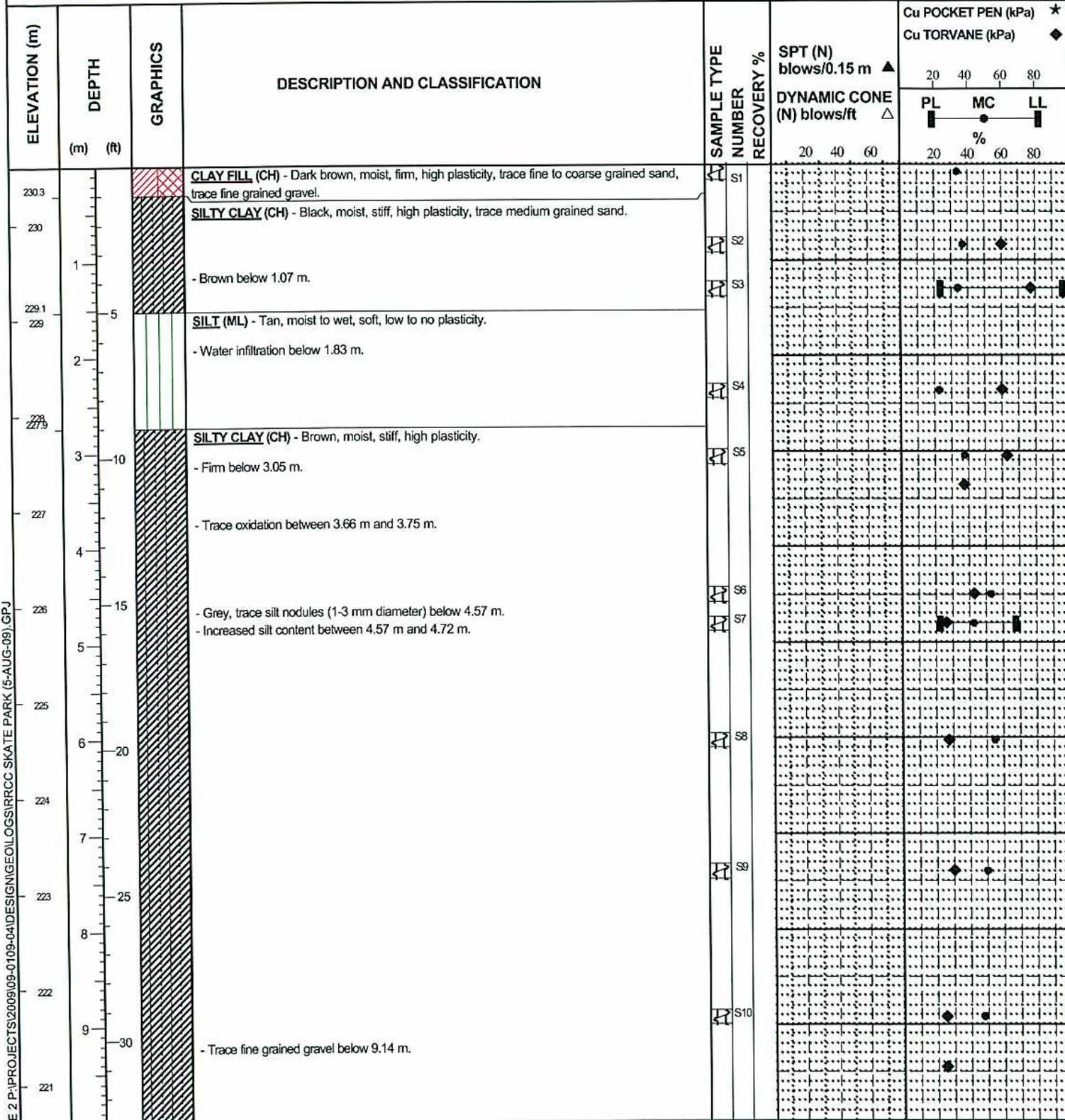
**JOB NO.** 09-0109-04  
**GROUND ELEV.** 230.7 m  
**TOP OF PVC ELEV.**  
**WATER ELEV.**  
**DATE DRILLED** 8/5/2009  
**UTM (m)** N 5,535,358  
 E 636,372

ELEVATION (m)	DEPTH (m) (ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE NUMBER	RECOVERY %	SPT (N) blows/0.15 m ▲	DYNAMIC CONE (N) blows/ft △	Cu POCKET PEN (kPa) ★			Cu TORVANE (kPa) ◆			
						20 40 60	20 40 60 80	PL	MC	LL	PL	MC	LL	
230.4			<b>CLAY FILL (CH)</b> - Black, moist, firm, crumbly, high plasticity, trace fine to coarse grained sand, trace fine grained gravel.	S1										
			<b>SILTY CLAY (CH)</b> - Black, moist, stiff, high plasticity. - Brown below 0.76 m. - Trace sand layers (1 mm thick), trace silt layers (1 mm thick) below 1.52 m. - Trace oxidation below 2.13 m.	S2										
228.4			<b>SILT (ML)</b> - Tan, moist to wet, soft, low plasticity, trace oxidation. - Water infiltration below 2.44 m. - No oxidation below 2.74 m.	S4										
227.7			<b>SILTY CLAY (CH)</b> - Mottled brown/grey, moist, firm, high plasticity, trace of silt nodules (1-3 mm diameter), trace silt lenses (1 mm thick).	S5										
224.6		<b>END OF HOLE AT 6.10 m</b>			S6									
		Notes: 1. 0.61 m of bentonite at the bottom, 0.61 m of bentonite at surface. Testhole backfilled with auger cuttings. 2. Testhole stayed open to bottom depth of 6.10 m at end of drilling. 3. Ground elevation was taken from survey data.												

SPT & TORVANE 2 P:\PROJECTS\2009\09-0109-04\DESIGN\GEOLOGS\RRCC SKATE PARK (5-AUG-09).GPJ

**CLIENT** SCATLIFF+MILLER+MURRAY  
**PROJECT** Red River Community Centre Proposed Skate Park Development  
**SITE** NE corner of Main St. & Ridgecrest Ave.  
**LOCATION** 39 m South of Ridgecrest Ave., 25 m West of Main St. (See Figure 1)  
**DRILLING METHOD** 125 mm ø Solid Stem Auger, CT 250 Canterra

**JOB NO.** 09-0109-04  
**GROUND ELEV.** 230.6 m  
**TOP OF PVC ELEV.**  
**WATER ELEV.**  
**DATE DRILLED** 8/5/2009  
**UTM (m)** N 5,535,384  
 E 636,375



SPT & TORVANE 2 P:\PROJECTS\2009\09-0109-04\DESIGN\GEOLOG\LOGS\RRCC SKATE PARK (5-AUG-09).GPJ

SAMPLE TYPE Auger Grab  
 CONTRACTOR **Paddock Drilling Ltd.** INSPECTOR **O. Wang**  
 APPROVED MRS. DATE 2/8/10

ELEVATION (m)	DEPTH		GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE NUMBER	RECOVERY %	SPT (N) blows/0.15 m ▲	Cu POCKET PEN (kPa) ★	Cu TORVANE (kPa) ◆
	(m)	(ft)					DYNAMIC CONE (N) blows/ft △	20 40 60 80	20 40 60 80
220	35				S11				
219									
218.4	40			END OF HOLE AT 12.19 m	S12				
218				<p>Notes:</p> <ol style="list-style-type: none"> <li>0.61 m of bentonite at the bottom, 0.61 m at surface. Testhole backfilled with auger cuttings.</li> <li>Testhole collapsed at 11.28 m below ground.</li> <li>Ground elevation was taken from survey data.</li> </ol>					
217	45								
216									
215	50								
214									
213	55								
212									
211	60								
210									
209	65								
	70								

SPT & TORVANE 2 P:\PROJECTS\2009\09-01\09-04\DESIGN\GEOLOGS\RRCC SKATE PARK (5-AUG-09).GPJ

SAMPLE TYPE Auger Grab

CONTRACTOR  
**Paddock Drilling Ltd.**

INSPECTOR  
**O. Wang**

APPROVED M.R.J. DATE 2/8/10

**CLIENT** SCATLIFF+MILLER+MURRAY  
**PROJECT** Red River Community Centre Proposed Skate Park Development  
**SITE** NE corner of Main St. & Ridgecrest Ave.  
**LOCATION** 27 m South of Ridgecrest Ave., 25 m West of Main St. (See Figure 1)  
**DRILLING METHOD** 125 mm ø Solid Stem Auger, CT 250 Canterra

**JOB NO.** 09-0109-04  
**GROUND ELEV.** 230.5 m  
**TOP OF PVC ELEV.**  
**WATER ELEV.**  
**DATE DRILLED** 8/5/2009  
**UTM (m)** N 5,535,387  
 E 636,387

ELEVATION (m)	DEPTH (m) (ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE NUMBER	RECOVERY %	SPT (N) blows/0.15 m ▲	DYNAMIC CONE (N) blows/ft △	Cu POCKET PEN (kPa) ★		Cu TORVANE (kPa) ◆	
								20	40	60	80
230.0	0		<b>CLAY FILL (CH)</b> - Brown/black, moist, firm, crumbly, high plasticity, trace fine to coarse grained sand, trace fine grained gravel, trace rootlets.	S1							
229.9	0.1		<b>SILTY CLAY (CH)</b> - Black, moist, stiff, high plasticity. - Brown below 1.10 m.	S2							
228.9	1.1		<b>SILT (ML)</b> - Tan, moist, soft, low to no plasticity.	S3							
228.5	1.5		<b>SILTY CLAY (CH)</b> - Mottled brown/grey, moist, firm, high plasticity, trace silt nodules. - Increased silt content between 2.13 m and 2.44 m.	S4							
227.9	2.1		<b>SILT (ML)</b> - Tan, moist, soft, low plasticity, trace clay nuggets (2-5 mm diameter).	S5							
227.4	2.6		<b>SILTY CLAY (CH)</b> - Mottled brown/grey, moist, firm, high plasticity, trace silt nodules (2-5 mm diameter).	S6							
227	3			S7							
226	4			S8							
225	5			S9							
224.4	5.6		<b>END OF HOLE AT 6.10 m</b>	S10							
224	6		Notes: 1. 0.61 m of bentonite at bottom, 0.61 m at surface. Testhole backfilled with auger cuttings. 2. No water in testhole at end of drilling. 3. Testhole stayed open to bottom depth of 6.10 m at end of drilling. 4. Ground elevation was taken from survey data.								
223	7										
222	8										
221	9										

SPT & TORVANE 2 P:\PROJECTS\2009\09-0109-04\DESIGN\GEO\LOGS\RRCC SKATE PARK (5-AUG-09).GPJ

SAMPLE TYPE Auger Grab

CONTRACTOR  
**Paddock Drilling Ltd.**

INSPECTOR  
**O. Wang**

APPROVED DATE 2/8/10

**CLIENT** SCATLIFF+MILLER+MURRAY  
**PROJECT** Red River Community Centre Proposed Skate Park Development  
**SITE** NE corner of Main St. & Ridgecrest Ave.  
**LOCATION** 41 m South of Ridgecrest Ave., 21 m West of Main St. (See Figure 1)  
**DRILLING METHOD** 125 mm ø Solid Stem Auger, CT 250 Canterra

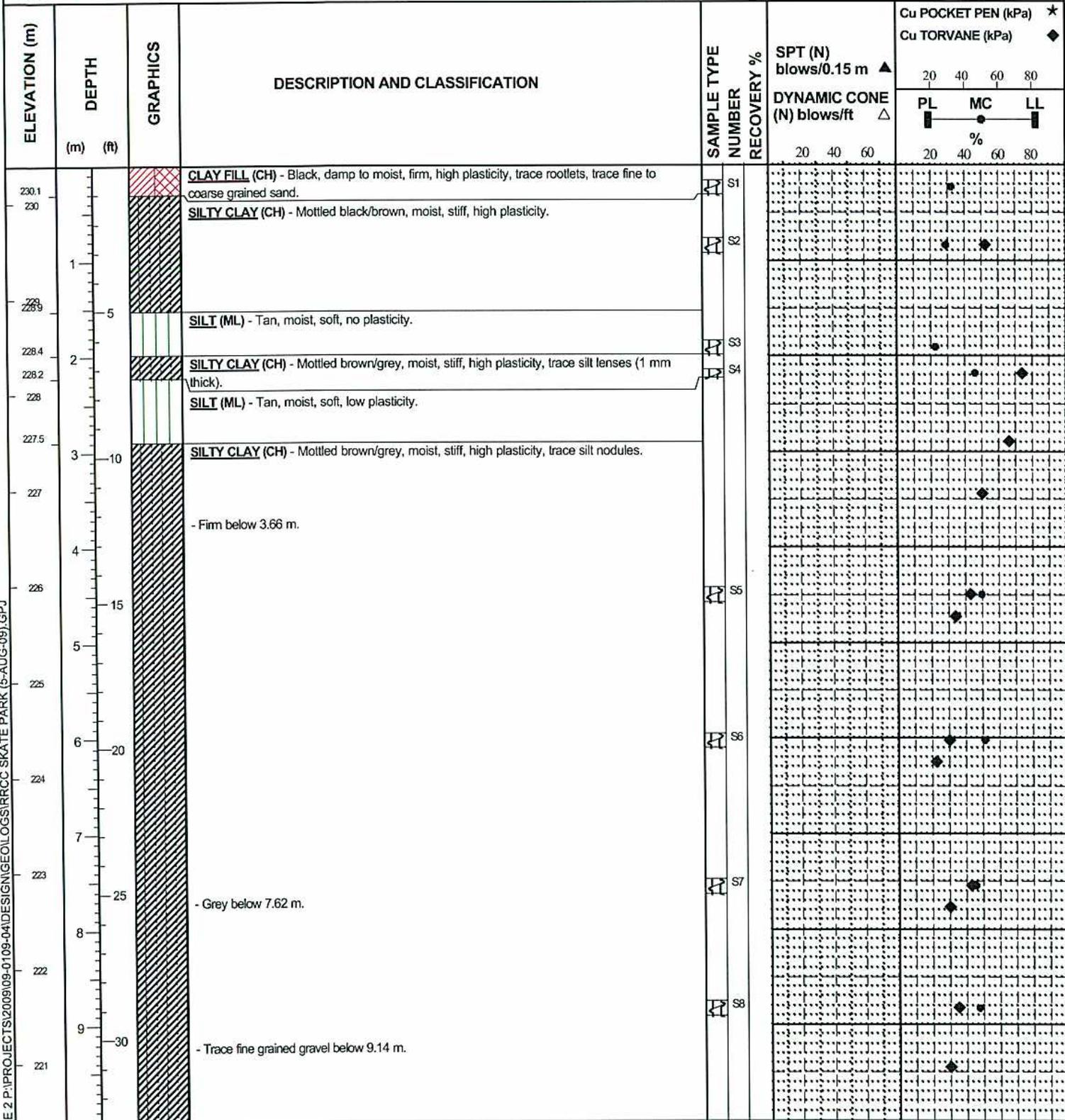
**JOB NO.** 09-0109-04  
**GROUND ELEV.** 230.6 m  
**TOP OF PVC ELEV.**  
**WATER ELEV.**  
**DATE DRILLED** 8/5/2009  
**UTM (m)** N 5,535,376  
 E 636,381

ELEVATION (m)	DEPTH (m) (ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE NUMBER	RECOVERY %	SPT (N) blows/0.15 m ▲	DYNAMIC CONE (N) blows/ft △	Cu POCKET PEN (kPa) ★	Cu TORVANE (kPa) ◆
						20 40 60	20 40 60	20 40 60 80	20 40 60 80
230.2			<b>CLAY FILL</b> - Black, dry, stiff, some fine to coarse grained sand, trace fine grained gravel.	S1					
230	1		<b>SILTY CLAY (CH)</b> - Mottled black/brown, moist, stiff, high plasticity, trace silt nodules (1-3 mm diameter).	S2					
229.0	5		<b>SILT (ML)</b> - Tan, moist, soft, low to no plasticity.	S3					
228.7			<b>SILT (ML)</b> - Tan, moist, soft, low to no plasticity.	S4					
228.4	2		<b>SILTY CLAY (CH)</b> - Mottled brown/grey, moist, stiff, high plasticity, trace silt nodules (1-2 mm diameter).	S4					
228			<b>SILT (ML)</b> - Tan, moist, soft, low to no plasticity.						
227.7	3		<b>SILTY CLAY (CH)</b> - Mottled brown/grey, moist, stiff, high plasticity, trace silt nodules (1-2 mm diameter). - Firm below 3.05 m.	S5					
227	10		- Increase silt content between 3.55 m and 3.66 m.						
226	15								
225	5								
224.5	6			S6					
224	20		<b>END OF HOLE AT 6.10 m</b>						
223	7		Notes: 1. 0.61 m of bentonite at the bottom, 0.61 m at the surface. Testhole backfilled with auger cuttings. 2. Water level measured at 4.27 m below ground at end of drilling. 3. Testhole stayed open to bottom depth of 6.10 m at end of drilling. 4. Ground elevation was taken from survey data.						
222	25								
221	8								
	9								
	30								

SPT & TORVANE 2 P:\PROJECTS\2009\09-0109-04\DESIGN\GEOLOG\LOGS\RRCC SKATE PARK (5-AUG-09).GPJ

**CLIENT** SCATLIFF+MILLER+MURRAY  
**PROJECT** Red River Community Centre Proposed Skate Park Development  
**SITE** NE corner of Main St. & Ridgcrest Ave.  
**LOCATION** 15 m South of Ridgcrest Ave., 19 m West of Main St. (See Figure 1)  
**DRILLING METHOD** 125 mm ø Solid Stem Auger, CT 250 Canterra

**JOB NO.** 09-0109-04  
**GROUND ELEV.** 230.4 m  
**TOP OF PVC ELEV.**  
**WATER ELEV.**  
**DATE DRILLED** 8/5/2009  
**UTM (m)** N 5,535,394  
 E 636,401



SPT & TORVANE 2 P:\PROJECTS\2009\09-0109-04\DESIGN\GEO\LOGS\RRCC SKATE PARK (5-AUG-09).GPJ

SAMPLE TYPE  Auger Grab

CONTRACTOR  
**Paddock Drilling Ltd.**

INSPECTOR  
**O. Wang**

APPROVED MRT. DATE 2/8/10

ELEVATION (m)	DEPTH (m) (ft)	GRAPHICS	DESCRIPTION AND CLASSIFICATION	SAMPLE TYPE	NUMBER	RECOVERY %	SPT (N) blows/0.15 m ▲	Cu POCKET PEN (kPa) ★
							DYNAMIC CONE (N) blows/ft △	Cu TORVANE (kPa) ◆
							20 40 60	20 40 60 80
							20 40 60	PL MC LL % 20 40 60 80
220	35		- Soft below 10.67 m.	S9				
219	40			S10				
218.2	40		END OF HOLE AT 12.19 m					
218			Notes: 1. 0.61 m of bentonite at the bottom, 0.61 m at surface. Testhole backfilled with auger cuttings. 2. No water in testhole at end of drilling. 3. Testhole squeezing between 1.54 m and 3.05 m below ground. 4. Testhole stayed open to bottom depth of 12.19 m at end of drilling.					
217	45							
216								
215	50							
214								
213	55							
212	60							
211								
210	65							
209	70							

SPT & TORVANE 2 P:\PROJECTS\2009\09-01\09-04\DESIGN\GEOLOGS\RRCC SKATE PARK (5-AUG-09).GPJ

SAMPLE TYPE Auger Grab

CONTRACTOR  
**Paddock Drilling Ltd.**

INSPECTOR  
**O. Wang**

APPROVED M.R.J. DATE 2/8/10