

APPENDIX A

GEOTECHNICAL REPORT

DYREGROV CONSULTANTS
CONSULTING GEOTECHNICAL ENGINEERS

**GEOTECHNICAL REPORT
SOUTH END WATER POLLUTION CONTROL CENTRE
PROPOSED EXPANSION**

Prepared for
STANTEC CONSULTING LIMITED
on behalf of
THE CITY OF WINNIPEG

**GEOTECHNICAL REPORT
SOUTH END WATER POLLUTION CONTROL CENTRE
PROPOSED EXPANSION**

**Prepared for
STANTEC CONSULTING LIMITED
on behalf of
THE CITY OF WINNIPEG**

February 2008

Project No. 272939

TABLE OF CONTENTS

1.0	INTRODUCTION	1
2.0	PROPOSED EXPANSION	1
3.0	SITE DESCRIPTION	1
4.0	BACKGROUND	2
5.0	FIELD INVESTIGATION	3
6.0	THE SOIL PROFILE	4
7.0	GROUNDWATER CONDITIONS	6
8.0	DISCUSSION AND RECOMMENDATIONS	7
8.1	General	7
8.2	Foundations	8
8.3	Excavations and Shoring	10
8.4	Below Grade Walls	11
8.5	Floor Slabs	12
8.6	Seismic Site Classification	12
8.7	Pavements	12
8.8	Other	13

Appendix

1.0 INTRODUCTION

This report summarizes the results of a geotechnical investigation undertaken by Dyregrov Consultants for the proposed expansion of the South End Water Pollution Control Centre. The area and extent of the proposed expansion is illustrated on Figure 1. The work was done at the request of Stantec Consulting Ltd. on behalf of the City of Winnipeg and was authorized by letter of July 19, 2007 under the signature of Mr. Cameron Dyck., P.Eng. Manager, Environmental Infrastructure.

2.0 PROPOSED EXPANSION

The long term expansion of the South End Water Pollution Control Centre is illustrated on Figure 1. It involves large concrete structures including Fermenters, Primary Clarifiers, Bioreactors, Secondary Clarifiers, Support Facilities and several lessor facilities. Also included is a parallel outfall discharge line to the Red River. Details of these facilities are provided in Section 8.1 of the Discussion and Recommendations Section 8.0. It is understood that not all of these facilities are planned to be constructed in the short term.

3.0 SITE DESCRIPTION

The site of the proposed expansion is south of the existing South End Water Pollution Centre (SEWPCC) with lesser works on the east side. The major portion of the site is flat lying with remnants of a snow dump area covering the easterly half of the site. Immediately to the west of the snow dump area is a spoil bank from excavations from the previous construction and is visually estimated to be about 4 to 5 metres in height. An area of dense bush and trees covers the westerly portion of the proposed development area. A number of drainage ditches are in the general area.

4.0 BACKGROUND

The original SEWPCC was constructed in the early 1970's. A major expansion was undertaken circa 1990 and a Disinfection Facility constructed in 1998.

Geotechnical studies were undertaken for the foregoing projects. The test holes and laboratory studies which were undertaken in these studies are included in the attached Appendix A. The reports which were referenced include the following:

* Ripley, Klohn & Leonoff International Ltd.
Report on Subsoil Investigation
Proposed South End Pollution Control Centre
Winnipeg, Manitoba
W - 580, March 8, 1971

* Ripley, Klohn & Leonoff International Ltd.
Report on Installation of Test Caissons
at South End Pollution Control Centre
Winnipeg, Manitoba
W - 619, March 24, 1971

* Ripley, Klohn & Leonoff International Ltd.
Test Holes Drilled at Outfall Stage
Associated with South End Pollution Control Centre
Winnipeg, Manitoba
W - 623, April 14, 1971

* Dyregrov and Burgess
Geotechnical Engineering Report
South End Water Pollution Control Centre
88528, April 15, 1988

* Dyregrov Consultants
Geotechnical Report
Proposed Disinfection Building
South End Water Pollution Control Centre
City of Winnipeg
981754, February 1998

5.0 **FIELD INVESTIGATION**

Between September 12 and 19, 2007, eighteen test holes were drilled in an area which covered the future plant expansion. The locations of the test holes are illustrated on Figure 1.

The test holes were advanced using truck-mounted drilling equipment which is owned and operated by Subterranean (Manitoba) Ltd. The test holes were either 450 mm or 125 mm in diameter. The deep test holes were carried to auger refusal in the glacial till which underlies the site. Shallow test holes were drilled to approximately 3 metres. Standpipe piezometers were installed in the 125 mm test holes which were carried to auger refusal. The soil profile was examined and classified on a continuous basis as the drilling progressed and sampled on a frequent basis. Disturbed samples were recovered from the auger cuttings and undisturbed samples were obtained in 75 mm Shelby tube samplers for laboratory testing.

Observations were made during the drilling with respect to groundwater, seepage and caving conditions encountered in the test holes. The sealed standpipe piezometers were installed in Test Holes 2007-02, 2007-08, 2007-09, 2007-11, 2007-15 and 2007-16A.

All of the test holes in which the piezometers were not installed were backfilled with excavated materials on completion.

The locations of the test holes were determined by Stantec Consulting Ltd. as well as the ground elevations at the test holes.

Test Holes 2007-12, 2007-13, 2007-14, 2007-20 and 2007-24 were not drilled for reasons of site access problems. Test Holes 2007-16 and 2007-18 could not be drilled at their respective locations due to access and were replaced by Test Hole 2007-16A.

6.0 THE SOIL PROFILE

Based on this investigation, the following describes the general soil profile at the site of the currently proposed development. The data from this investigation is generally consistent with the data from previous investigations.

A thick deposit of highly plastic Lake Agassiz lacustrine silty clay is the predominant component of the soil profile which extends from the ground surface to depths varying from 12.5 to 16.0 metres. The average thickness is approximately 14.3 metres. The clay is common to the Winnipeg area and can be described as firm to stiff in relative consistency. Moisture contents are typically within the 40 to 60 percent range and are relatively uniform with depth. Moisture depletion appears to be restricted to about the upper 3 metres of the soil profile. Plastic and Liquid Limits for the clays are in the order of 30 and 100 percent, respectively, and the Liquidity Indices at this location are estimated to be in the range of 0.3 to 0.4. It should be noted that specific tests were not performed for the determination of these index properties from samples recovered in this recent investigation.

Undrained shear strengths were determined from unconfined compression tests, pocket penetrometer and Torvane tests in the laboratory. A plot of the undrained shear strength profile versus depth is provided as Figure 20. The lower strengths from the unconfined compression tests within the upper 3.6 metres of the profile are probably related to secondary defects (fissuring) that has accompanied moisture depletion within these depths. There is a trend in decreasing strengths with depth.

Covering the site are variable thicknesses of fill, remnant debris from the snow dumps and topsoil. The thickness of these materials, which generally consists of silt, sand and gravel, were as

thick as 1.22 metres. This is exclusive of the stockpile of excavated materials from the earlier developments. Also, the area of trees and brush will contain organic topsoil and roots.

Near the upper part of the clay profile, in 8 of the 18 test holes, was a silt layer of variable thicknesses up to 1.22 metres and depths between 0.3 and 1.98 metres. It was tan in color, moist to wet and loose to firm in consistency.

The silty clays are underlain by a glacial silt till deposit. The glacial till is known to be a heterogeneous mixture of sand, gravel, cobble and boulder size materials within a predominately silt matrix. The relative density of the glacial till has been evaluated on the basis of its moisture content and visual examination of the auger cuttings. The elevation of the surface of the glacial till varies from about 214.62 to 220.33 metres. The average elevation is 218.72 metres. The glacial till is typically loose or soft near its surface and becomes more dense with depth, however, caving conditions were encountered within the glacial till deposit which prevented recovery of suitable samples for evaluation. The test holes were advanced by screwing the auger until it met refusal on very dense glacial till or boulders in the till. The action of the drill rig did not suggest the presence of the bedrock, but it could be present. The materials through which the augers were drilled are believed to be layered deposits of fine sand and glacial deposits. Some fine sands were actually recovered. Auger refusal was reached between elevations 208.45 and 213.98 metres.

A detailed description of the soil profile and the results of the field and laboratory testing are summarized on the test hole logs, Figures 2 to 19. The logs from previous studies are included in the Appendix.

7.0 GROUNDWATER CONDITIONS

The groundwater conditions at the site consist essentially of groundwater perched within the relatively pervious silt strata that are within the upper part of the soil profile and a subartesian condition within the underlying glacial till and bedrock.

Groundwater conditions in the upper silt deposits are likely to vary over short distances, since they are not contiguous across the site. Seasonal precipitation will influence the groundwater conditions in the silt.

Piezometric pressures within the glacial till deposit originate in the underlying limestone bedrock, which is the carbonate aquifer that is common to Winnipeg, and these are the most relevant to the construction of relatively deep or large excavations. The standpipe piezometers were installed in Test Holes 2007-02, 2007-08, 2007-09, 2007-11, 2007-12, 2007-15 and 2007-16A with their tips sealed into the glacial till. These were installed to determine the elevation of the piezometric surface within the glacial till deposit. The following table shows the groundwater levels which were taken at the time of installation and 8 days later. The piezometric elevations about one week after installation were between 223.79 and 224.41 metres.

Groundwater Elevations (m)			
Piezometer	September 18, 2007	September 19, 2007	September 26, 2007
2007-2	-	223.18	224.33
2007-8	-	224.38	224.15
2007-9	-	223.83	224.41
2007-11	222.99	223.90	224.13
2007-15	221.66	223.49	223.79
2007-16A	221.55	223.92	224.30

Attached as Figures 21 and 22 are the test hole log and hydrograph from the Provincial Groundwater Monitoring Well G05OC0097 which is located in the basement of the SEWPCC. It is noteworthy from the hydrograph that there has been a trend toward higher groundwater levels since the time of the initial construction in 1970 and since the major expansion about 1990. The annual peaks, which are frequent, are apparently associated with Floodway events. As indicated on the hydrograph, the only time in the last 10 years that the bedrock groundwater pressures have risen above 225.0 metres was during the major Floodway operation events of 1997 and 2006.

8.0 DISCUSSION AND RECOMMENDATIONS

8.1 General

The long term additions which are proposed are illustrated on Figure 1. Some of the additions are expected to be similar to some of those that presently exist. The proposed facilities include:

- Preliminary Treatment Expansion will include grit removal tanks which will be comparable to those that presently exist and will be approximately 6.0 metres deep below finished grade at approximately elevation 228.0 metres. They will always contain fluids except when taken out of service for cleaning.
- Standby Power Building will be on grade and will house one or more generators.
- Primary Clarifiers, one of which will be constructed initially, will have a footprint of 45 by 15.6 metres and 5.0 metres in depth (approx. elev. 228.9 metres with a sludge hopper that extends 3.4 metres deeper (elev. 225.5 metres). The clarifiers will maintain fluid except when taken out of service for cleaning.
- Bioreactors will be constructed adjacent to the existing bioreactor and it is anticipated that the floor of the reactors will be at the same elevation as the existing which is 228.1 metres. The four new bioreactors will be 44.1 by 33.9 metres by 6.7 deep. They will be full of fluid at all times except when taken out of service for cleaning.
- Blower/Electrical/Workshop/Odour Control/Alum/Chlorine Rooms will be adjacent to the Bioreactor tanks. These rooms will be at grade, some of which may contain heavy equipment/storage tanks.

- Secondary Clarifiers, two of which are proposed to be constructed initially, will have diameters of 45.7 and 33.5 metres. The depths of the clarifiers will be about 5.1 metres with a central core to a depth of 7.6 metres (elev. 225.0). The clarifiers will be maintained full except for when taken out of service for cleaning.
- The U/V Disinfection Facility will be twinned with the existing facility. It will be 25 metres in length, 5.4 metres in width and to a depth of 3.9 metres (elev. 229.0).
- Fermenters will each be 21.3 meters in diameter and will be partially buried. Adjacent to the fermenters will be a DAF Room/truck Bay/Electrical Room/Odour Control Room/ Sludge Holding Tank all of which will be at grade. The DAF room will include four above ground process tanks, each tank approximately 8.1 by 2.6 metres and 2.5 metres high. The sludge holding tank room will contain three above ground sludge tanks, each being about 20 by 9 metres and 2.5 metres high.

8.2 Foundations

The geotechnical conditions are best suited to the use of hexagonal, prestressed, precast concrete piles that are driven to practical refusal in the underlying glacial till. These have been the type of pile which has been used to support the majority of the structures for the existing plant. The variable condition of the glacial till deposit and the potential problems related to water seepage and bell instability are factors that render the site unsuitable for widespread use of high capacity cast-in-place concrete caissons and this type of foundation is not recommended.

The driven end bearing precast concrete piles can be assigned conventional capacities of 445, 625 and 800 kN for 305, 356 and 406 mm sizes respectively if driven to practical refusal with diesel hammers with a rated energy of not less than 40,000 Joules. Practical refusal can be defined as final penetration resistance values of 5, 8 and 12 blows per 25 mm or less for 305, 356 and 406 mm diameters respectively for the final 3 sets of pile penetration for hammers with driving energies of 40,000 Joules. If higher energies or other types of hammers are used, they should be evaluated to ensure that the piles are not overstressed and a suitable refusal criteria determined.

Construction practice in Winnipeg normally includes preboring at all driven pile locations usually to diameters that are 50 mm greater than the pile size and to depths of about 3 metres. The preboring is effective in reducing ground vibrations, pile heave and contributes positively to pile verticality. No reduction in individual pile capacity is necessary for reasons related to group action provided that pile heave is monitored, measures are taken to minimize it (preboring) and redriving is done, as necessary, in pile groups. Redriving of all piles in groups should be specified. Piles should not be spaced closer than 2.5 pile diameters centre to centre. Full time pile inspection is recommended for the driven pile installations.

The age of the precast pile concrete should be specified to be at least seven days old prior to driving.

Lightly loaded structures can be supported on cast-in-place concrete friction piles which can be designed on the basis of an allowable shaft adhesion value of 19.2 kPa. The top 3.0 metres of shaft support should be discounted due to potential soil shrinkage away from the pile. A minimum pile diameter of 405 mm should be specified. Temporary casings should be used on an as-required basis, to prevent caving and seepage into the pile borings.

A mixture of friction piles and end bearing piles is not recommended for the support of important structures, nor should groups of friction piles be used for large loads.

Any foundations which might be affected by freezing conditions should be protected from frost heave effects. The use of flat lying rigid insulation, such as Styrofoam HI, can be used to prevent frost penetration into the soil around the piles. Alternatively, the pile lengths should be a minimum of 7.6 metres and should contain full length reinforcement regardless of the design loads.

8.3 Excavations and Shoring

Deep excavations will be required for most of the major structures which may be in open areas and others adjacent to existing facilities. In the open areas, it may be possible to use sloped excavations. Adjacent to the existing facilities, shoring may be required. Because these options will impact on the construction activities and schedules, it is recommended that the successful contractor be required to submit an excavation and shoring plan which should be prepared by or endorsed by a registered Professional Engineer who is skilled in these matters.

The excavation and shoring plan should consider the potential for bottom heave of the deeper excavations due to hydrostatic pressures within the underlying glacial till deposit and bedrock. As noted in Section 7.0, the highest groundwater elevations which have been recorded at the site occurred during the Floodway events which, in 2006, were as high as 226.8 metres. With this groundwater elevation, the maximum depth of excavation to elevation 224.5 metres and the highest elevation of the glacial till (or bottom of the clay deposit), the Factor of Safety against bottom heave is too low. It should be appreciated that all of the foregoing are the extremes of the limits which could be used for the analyses. In general, exclusive of the periods of the Floodway events, the Factors of Safety appear to be adequate, however, the development of the excavation and shoring plan should assess the base heave potential for the deeper excavations.

The design of the excavation slopes should consider the soil stratigraphy and piezometric conditions which might prevail at the time of construction. The presence of the silt deposit should be recognized as sloughing and seepage should be expected during periods of heavy rainfall. The excavation slopes should be immediately protected from drying by covering with suitable materials. Particular attention should be paid to excavation slopes where the new excavations will encroach upon or expose the existing structures.

Temporary shoring should be provided where excavations will encroach on structures that have to be protected. The shoring can be designed on the basis of the earth pressure distribution shown on Figure 23. Ground movement behind the shoring will occur and is largely unavoidable. The amount that will occur cannot be predicted with much accuracy, mainly because the movement is as much a function of excavation procedures and workmanship as it is a function of theoretical considerations.

8.4 **Below Grade Walls**

Below grade walls including the tanks and any retaining walls should be designed to resist lateral earth pressures that are derived on the basis of the following conventional relationship which produces a triangular pressure distribution:

$$P = K \lambda D$$

where P = lateral earth pressure at depth D (kPa)

K = earth pressure coefficient (0.5)

λ = soil/backfill unit weight (17.3 kN/m³)

D = depth from surface to point of pressure calculation

The base of the wall should be provided with a filter protected drainage system to prevent the buildup of hydrostatic pressures against the wall. Where drainage is not provided, the hydrostatic pressure should be included assuming a water table to be at the ground surface. The selection of backfill materials should be reviewed during the design and their impact on the foregoing pressures reassessed.

An allowance for surface live loads should be included if a significant load is applied within a distance from the wall equal to the height of the wall. The lateral earth pressure due to the live load should be presumed to be equal to 50 percent of the vertical pressure due to the live load.

8.5 Floor Slabs

Structurally supported floor slabs, generally, should be used throughout. These slabs should be separated from the underlying subgrade by a void of at least 200 mm. It is presumed that the slabs will not be provided with underdrainage and that water can collect beneath them. This is conducive to swelling and heave and a generous allowance for this is recommended.

8.6 Seismic Site Classification

On the basis of a weighted undrained shear strength of the clay profile of 55 kPa, the site falls into Site Class D of the Site Classification for Seismic Site Response of the 2005 NBCC.

8.7 Pavements

Pavement structures should be placed on a prepared subgrade. The silty clay which is below the topsoil and fill (which should be removed and stockpiled or wasted) is a suitable subgrade material. It should be reworked until the moisture content is near its optimum value. It would then be compacted to a uniform density of at least 95 percent of Standard Proctor Density. Any "soft spots" which develop during the subgrade preparation should be subcut and replaced with suitably compacted clay materials. Where silt is encountered, it should be subcut by 750 mm and bridged with a granular fill. A woven geotextile should be placed between the native soil and the granular fill to provide a separation and reinforcement.

On the prepared subgrade the pavement areas for parking and light duty traffic should consist of 50 mm of asphaltic concrete placed on 210 mm of crushed granular base course and for heavy duty traffic for trucking, it should consist of 76 mm of asphaltic concrete on 460 mm of crushed granular base course, or equivalent sections. Concrete pavements would entail 205 mm of reinforced concrete on 75 mm of crushed granular base course.

The materials selection and construction requirements should be to the standards of road construction as set out in the City of Winnipeg Standard Specifications.

8.8 Other

All concrete in contact with the soil should be manufactured with sulphate resistant cement and should be of high quality.

Respectfully submitted,

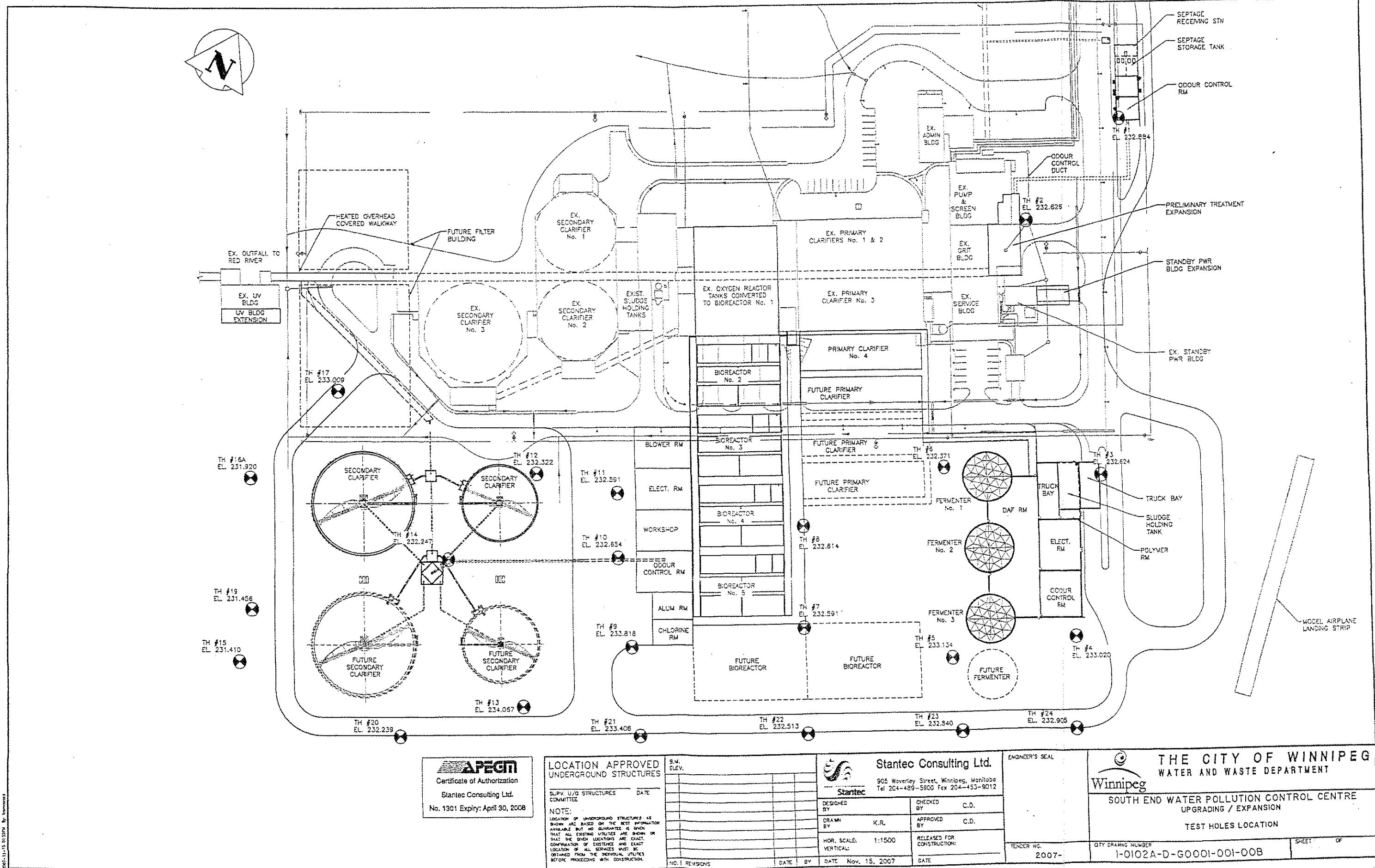
DYREGROV CONSULTANTS

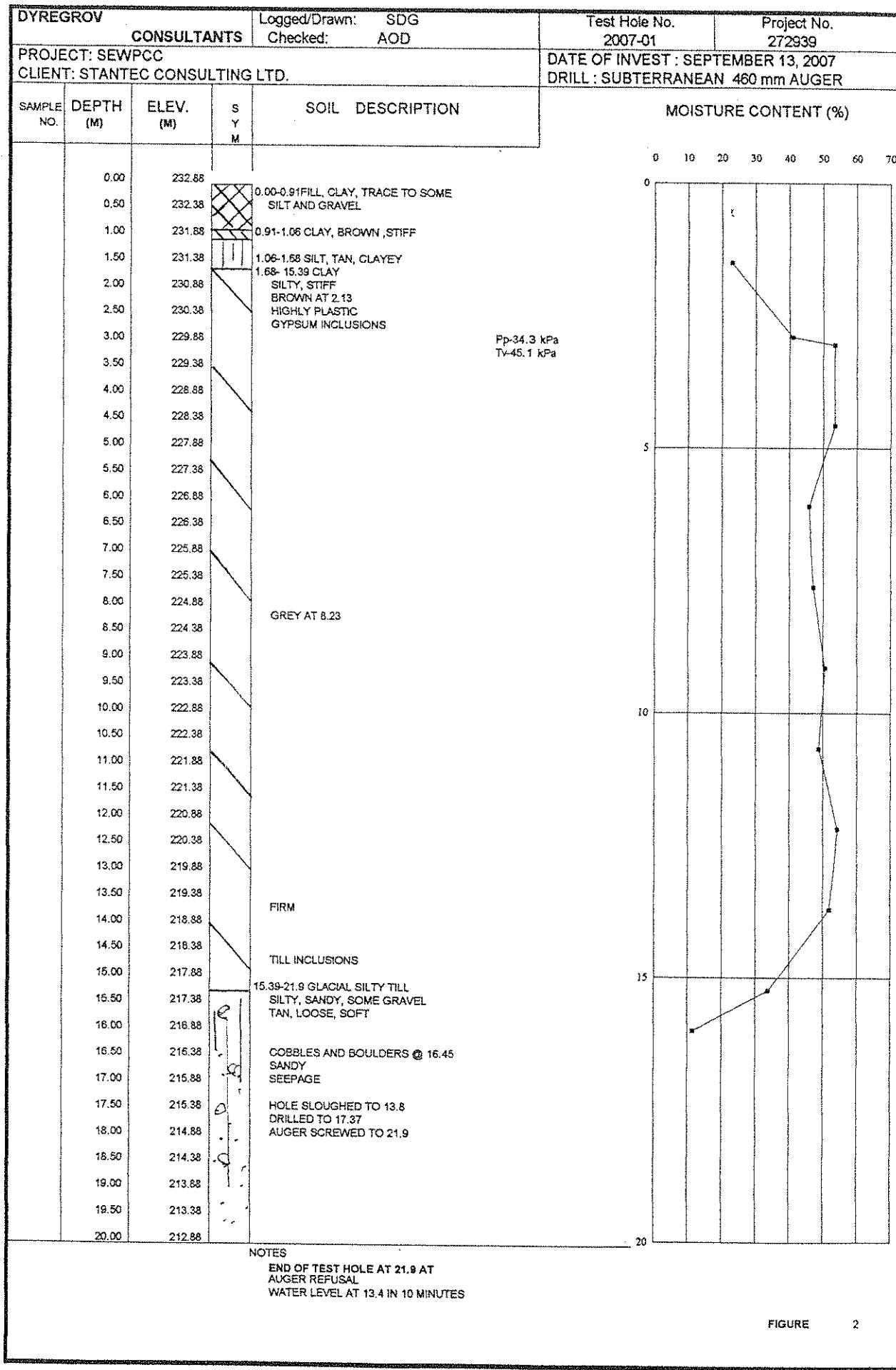


Per:



A.O. Dyregrov, P.Eng.





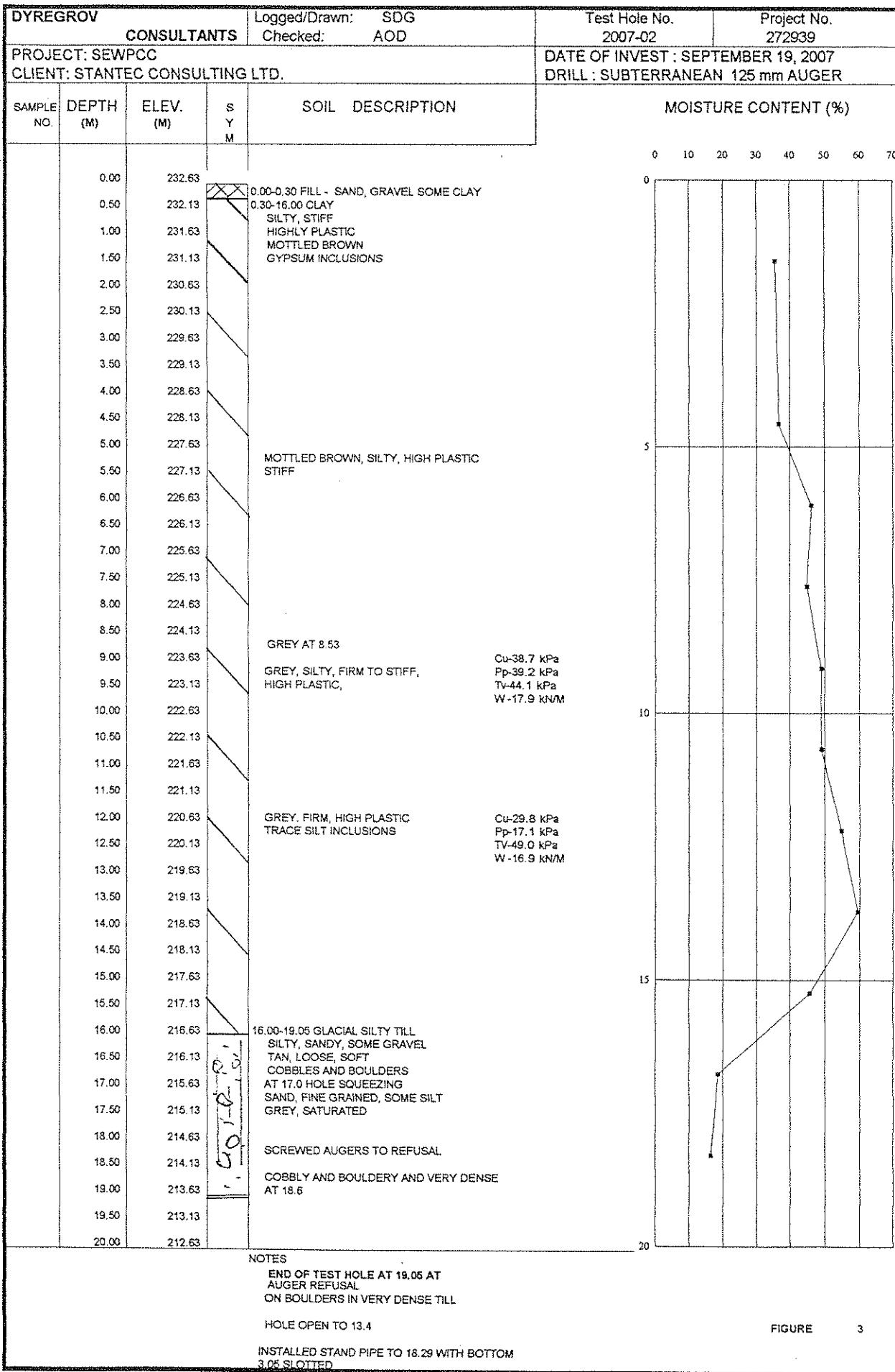
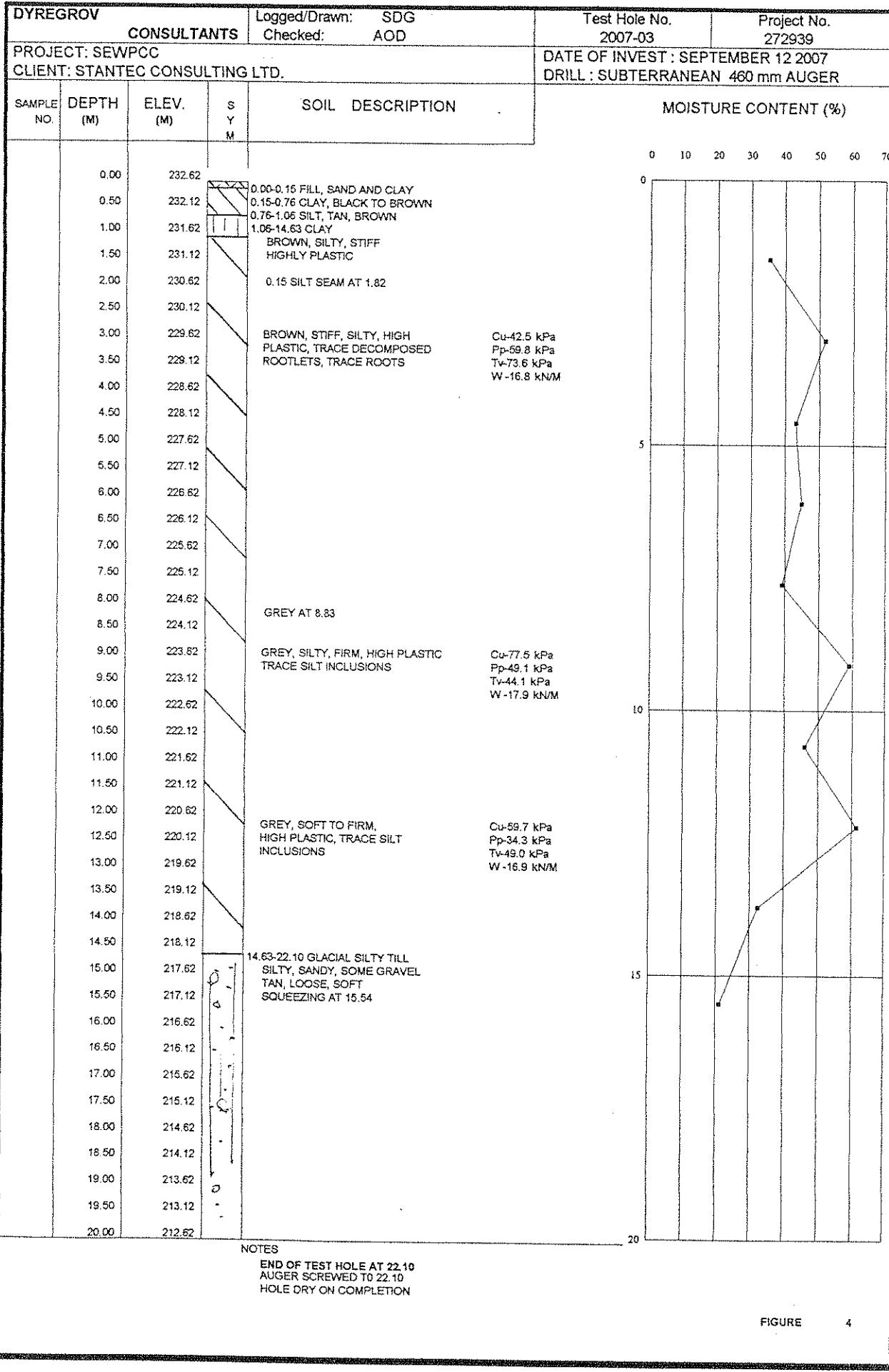
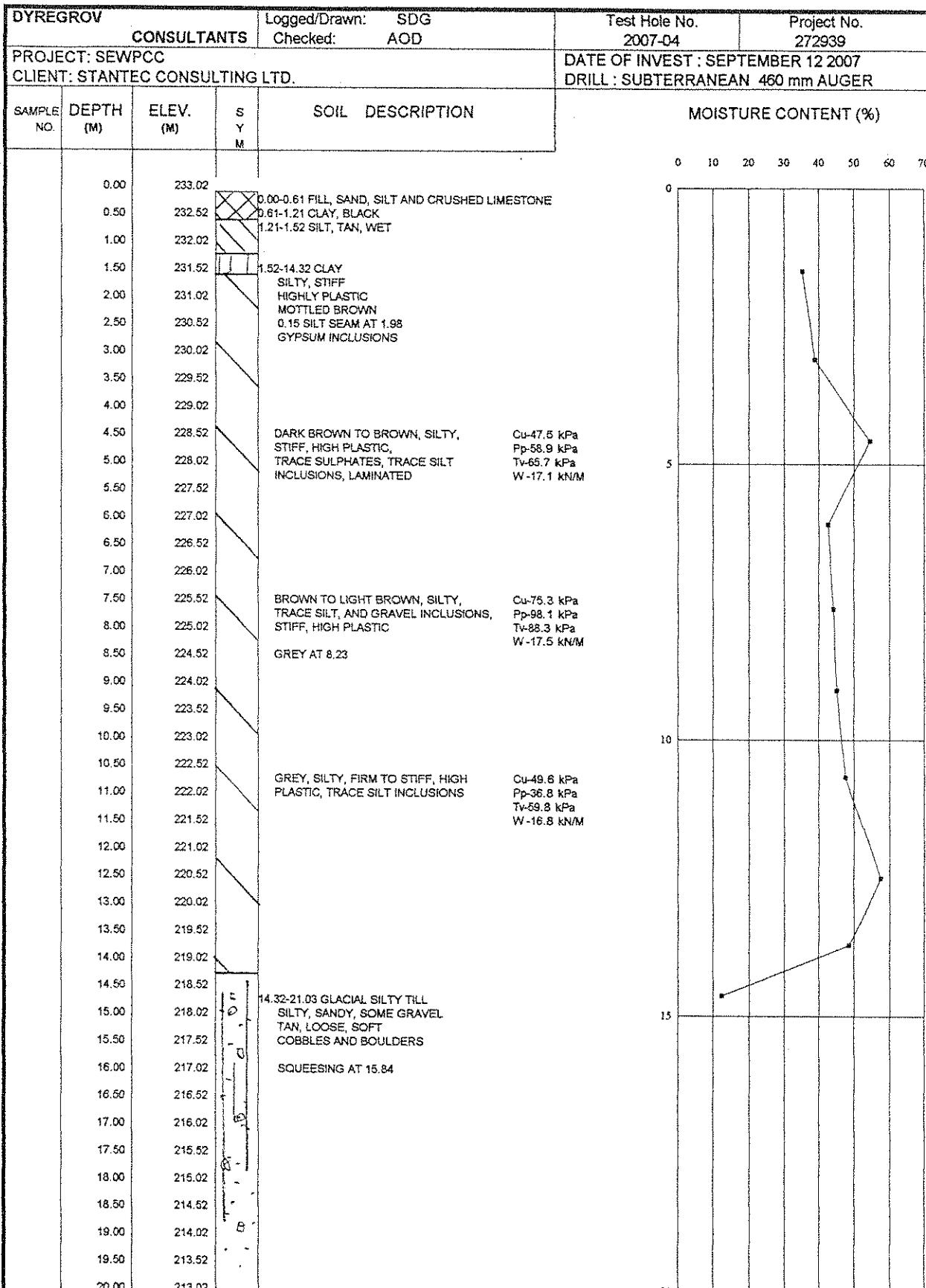
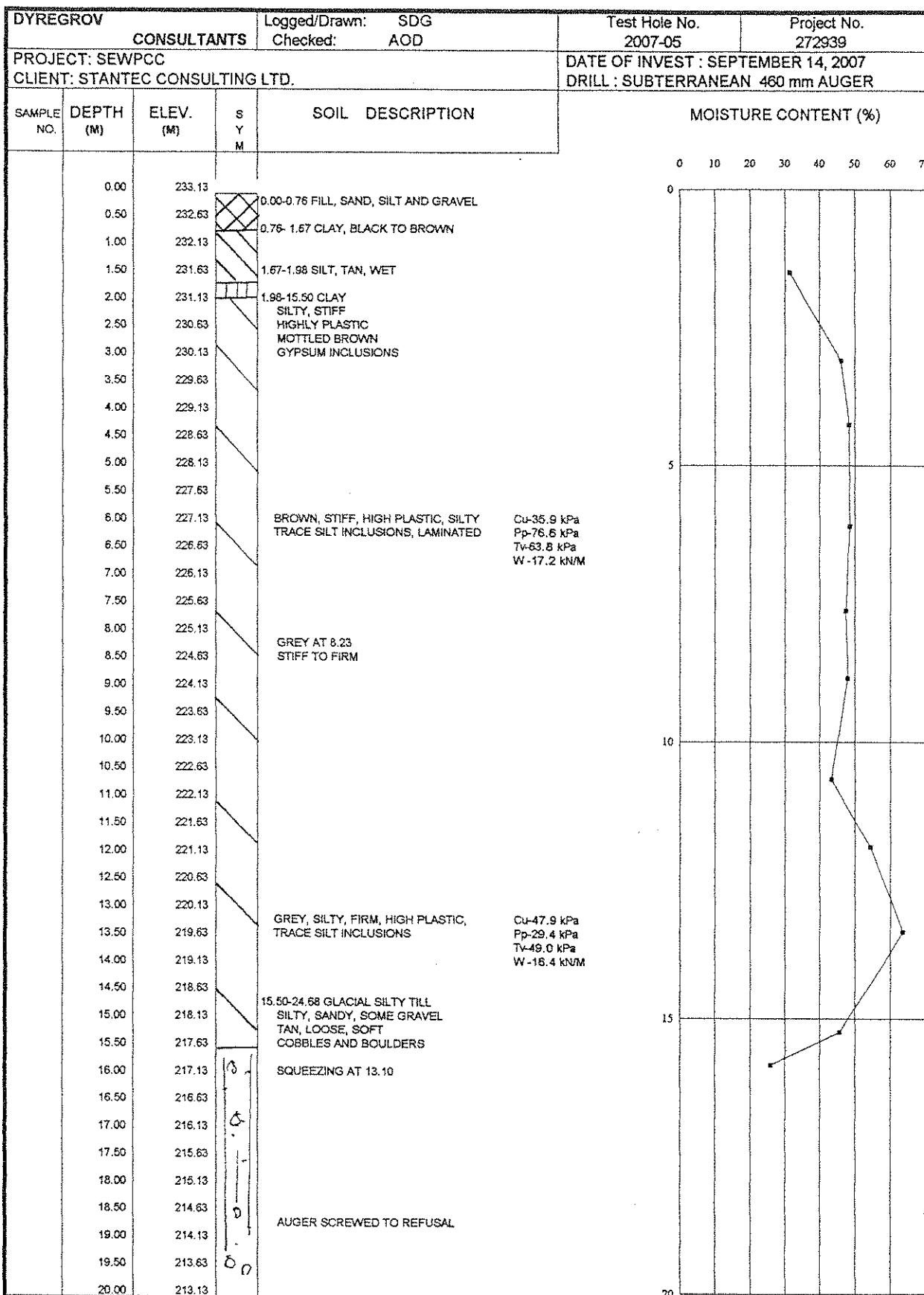
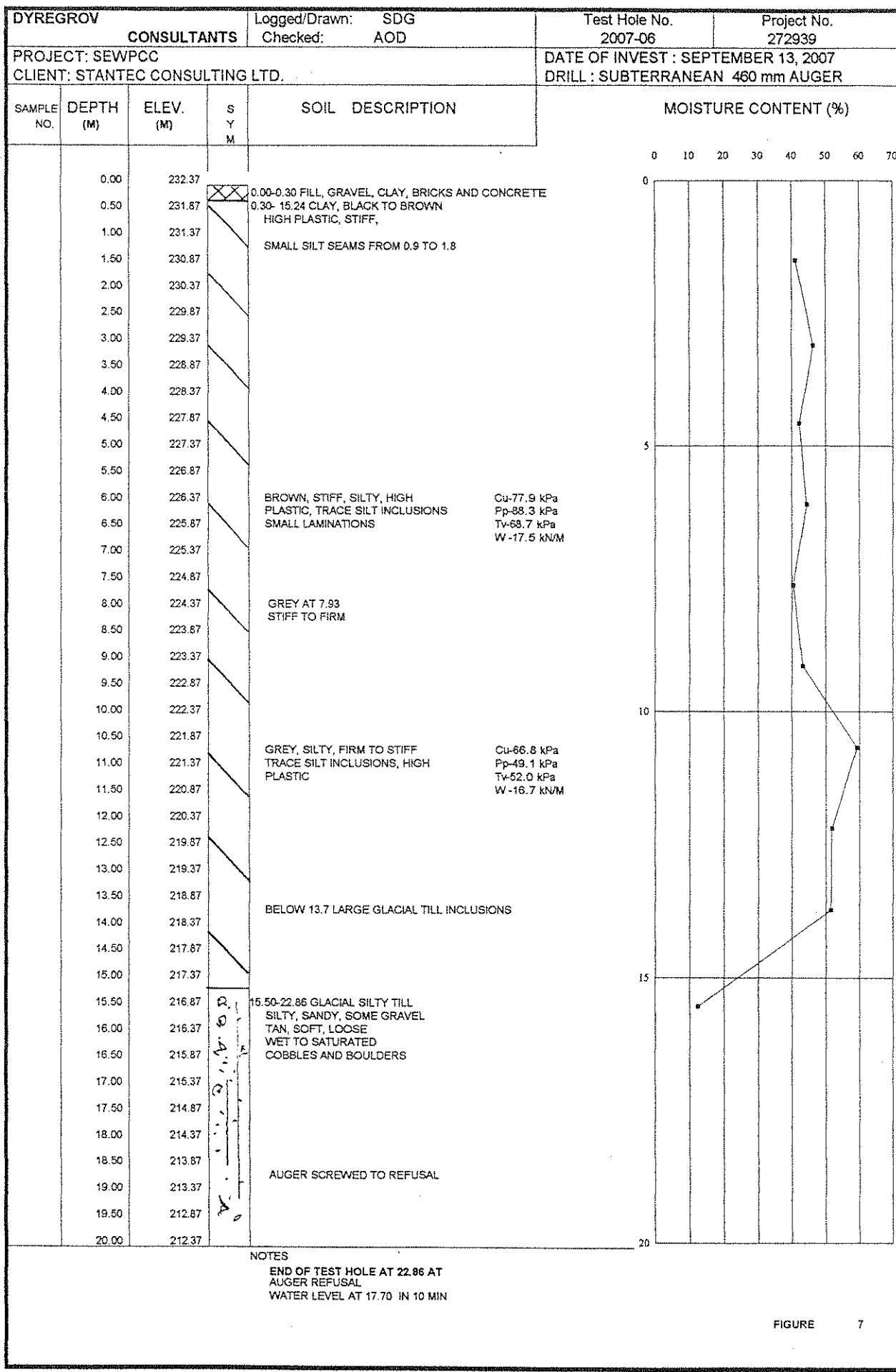


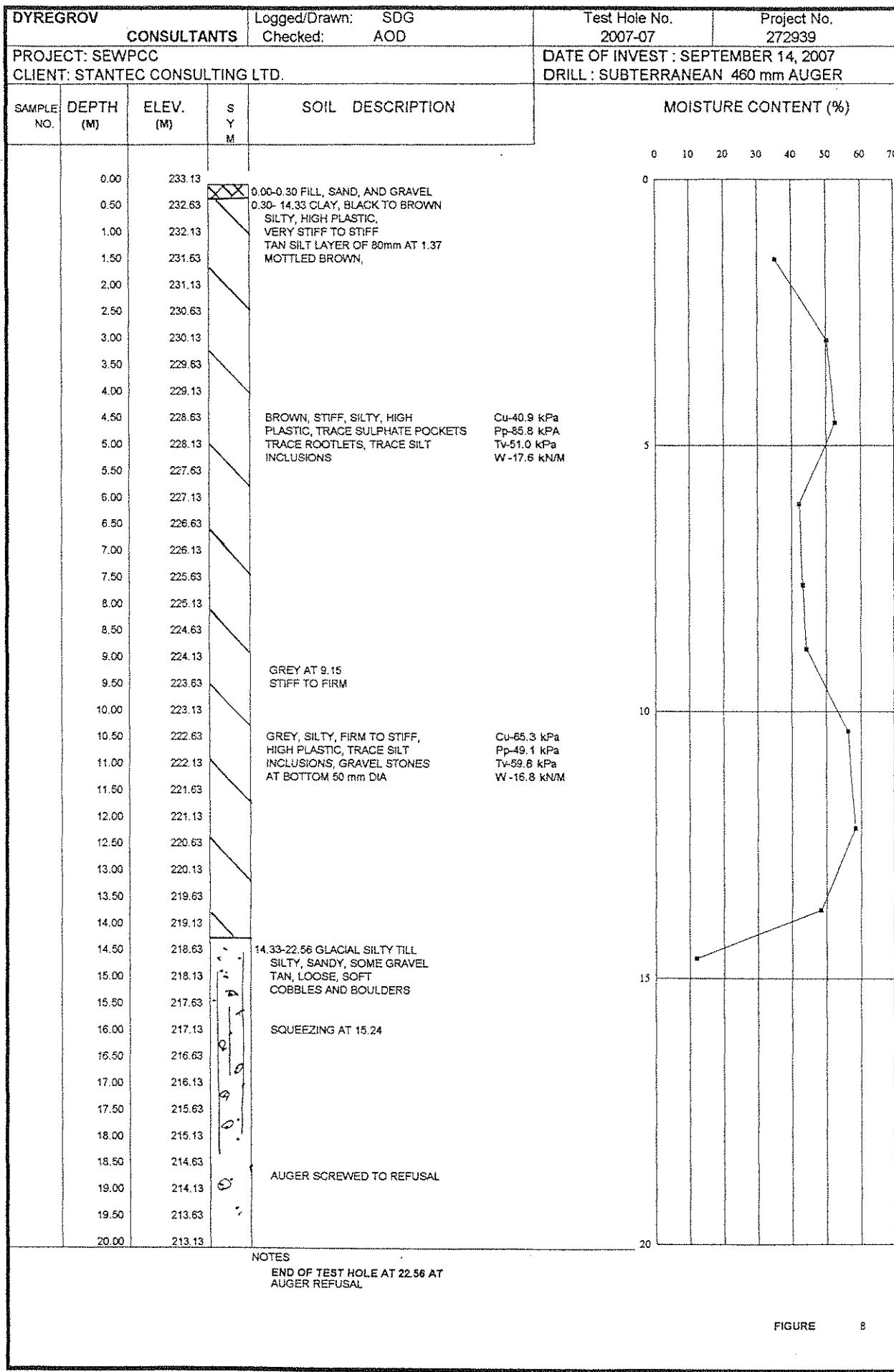
FIGURE 3

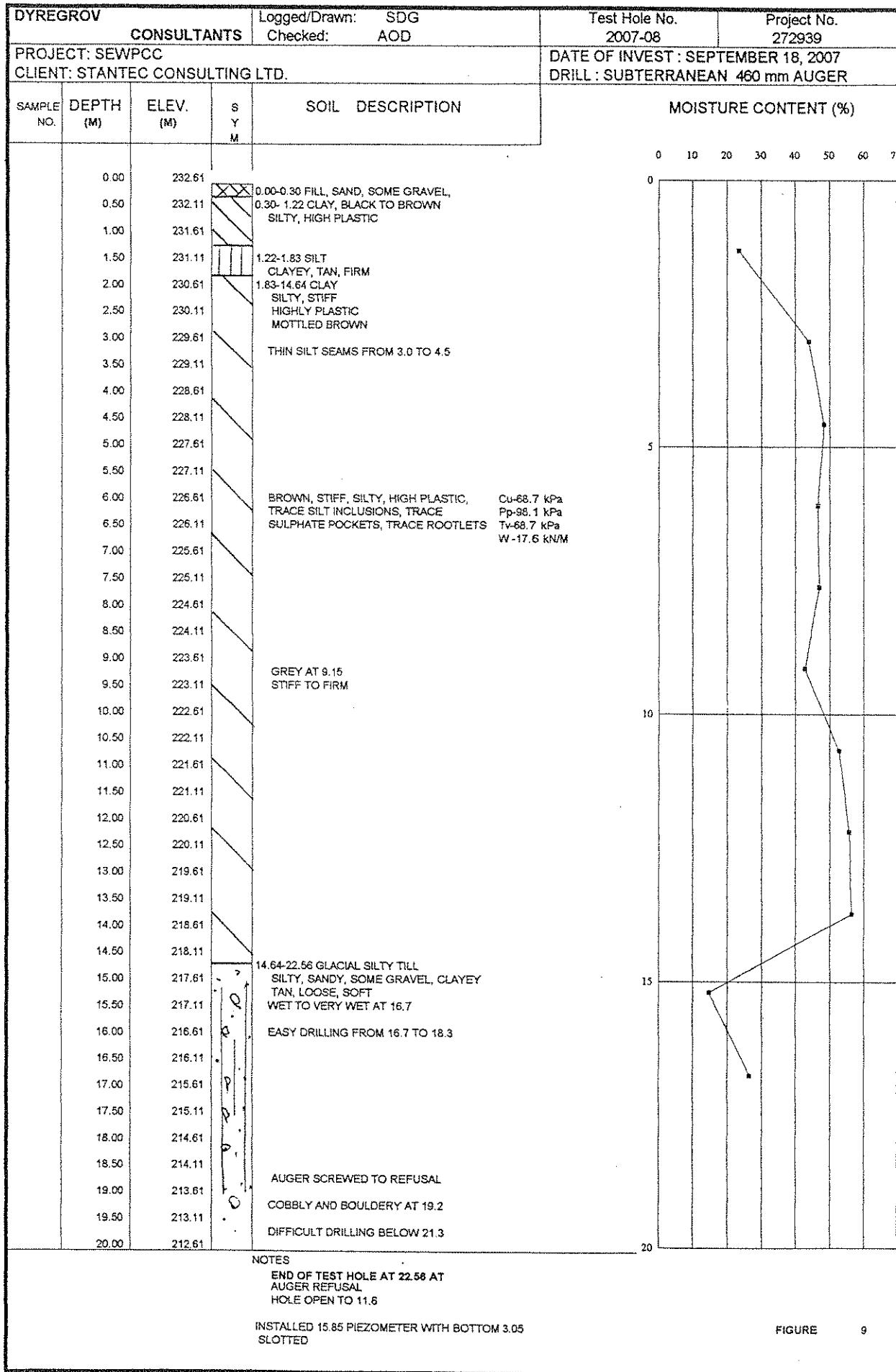


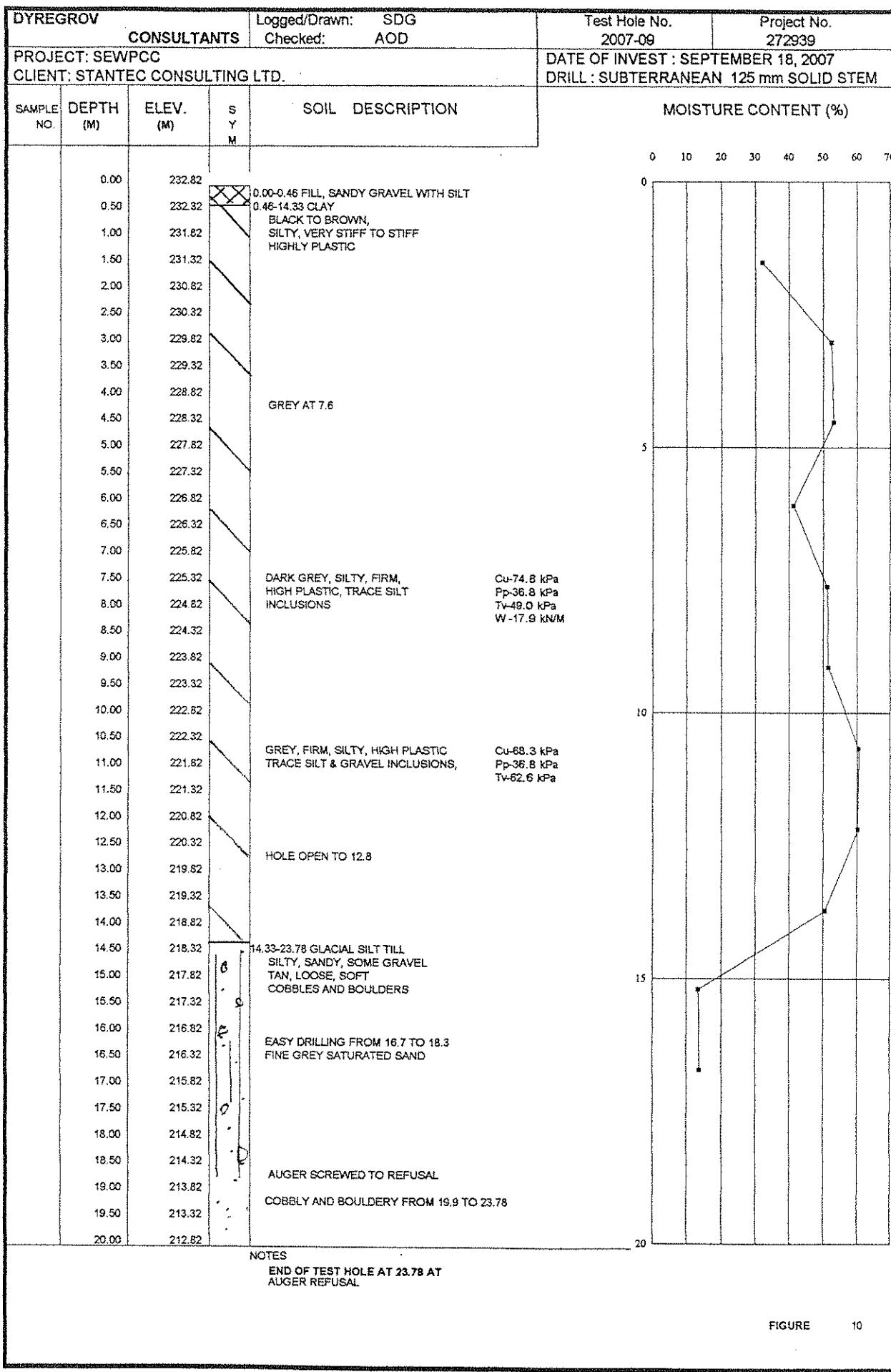


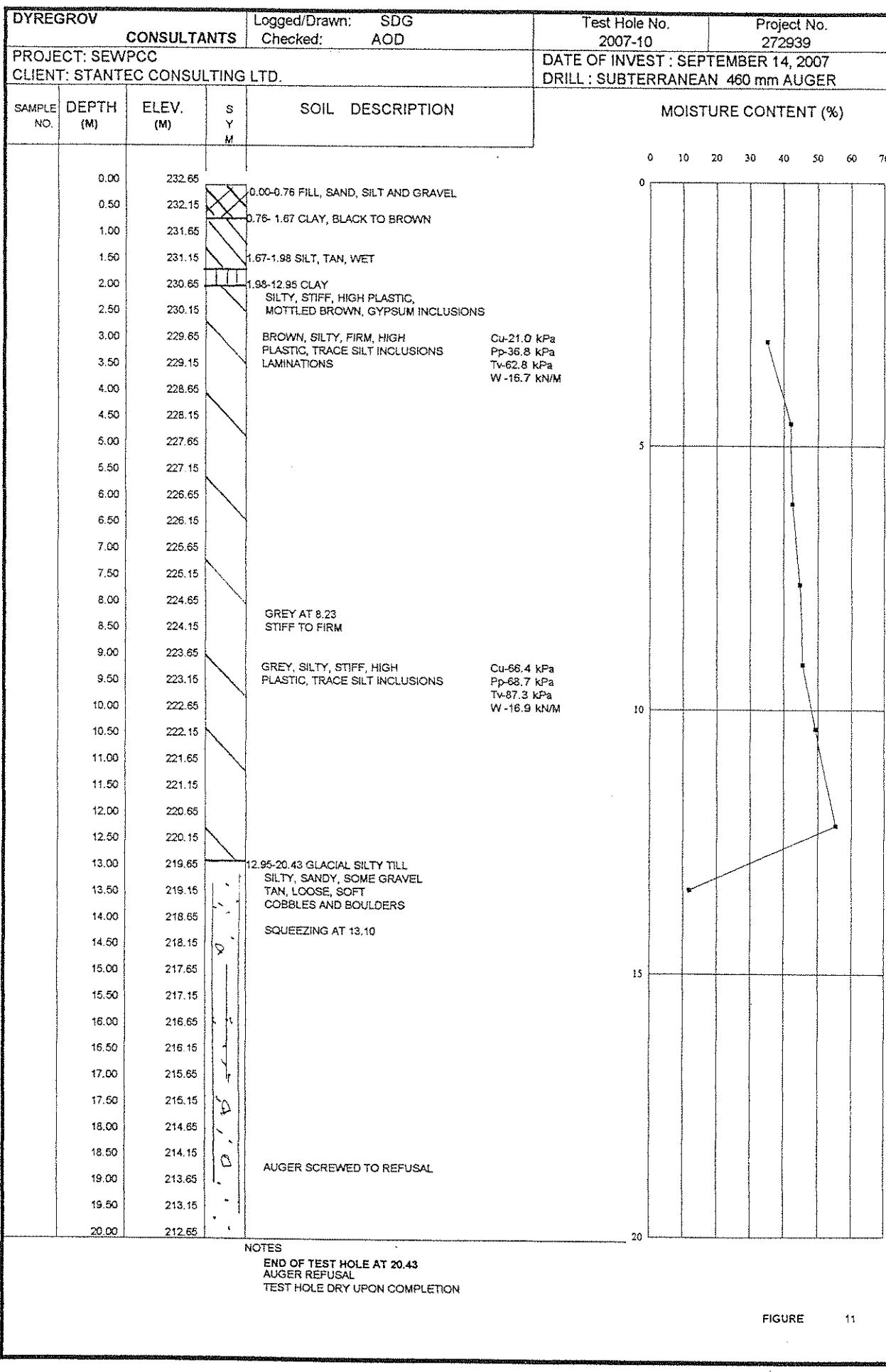


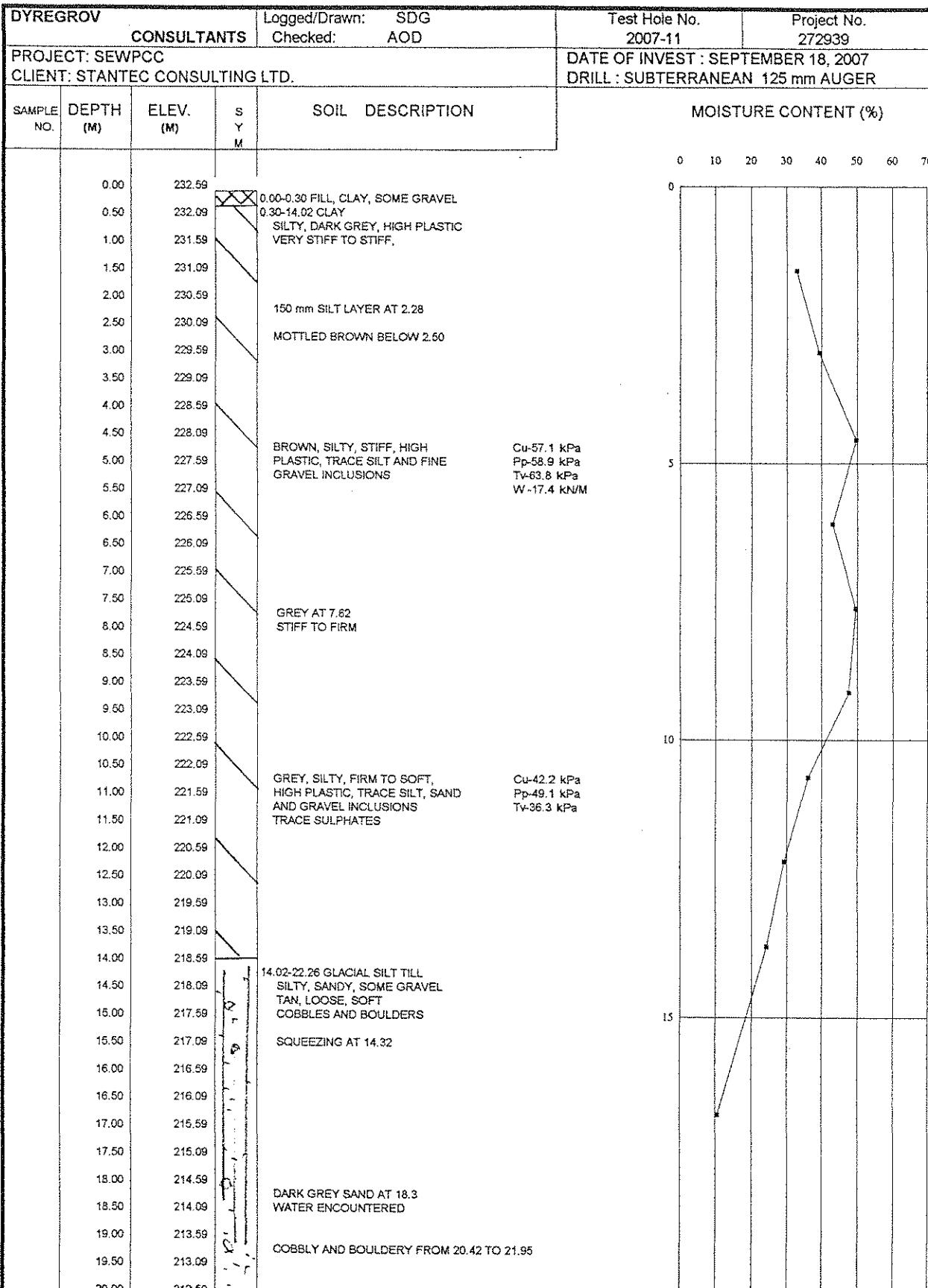


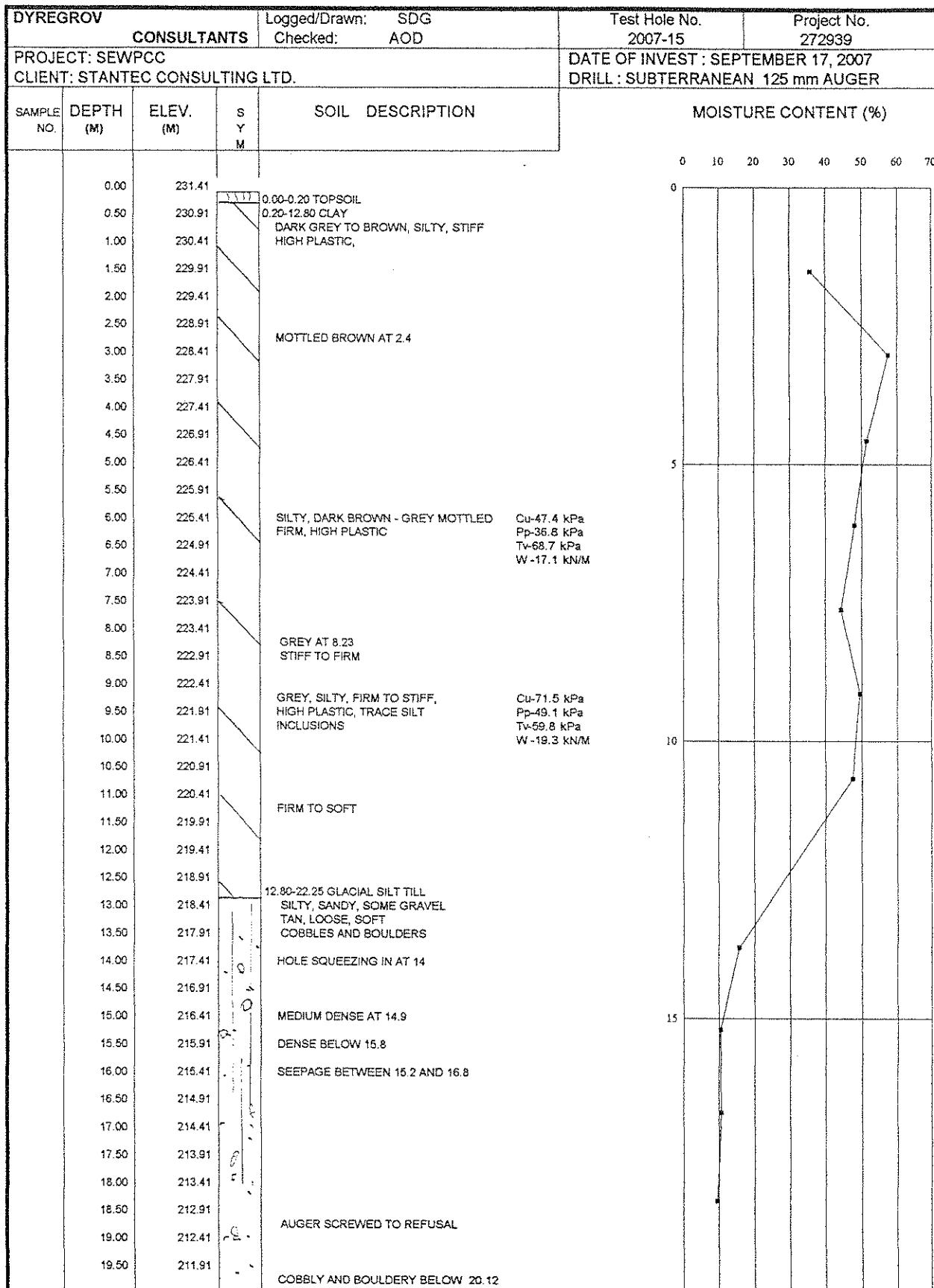












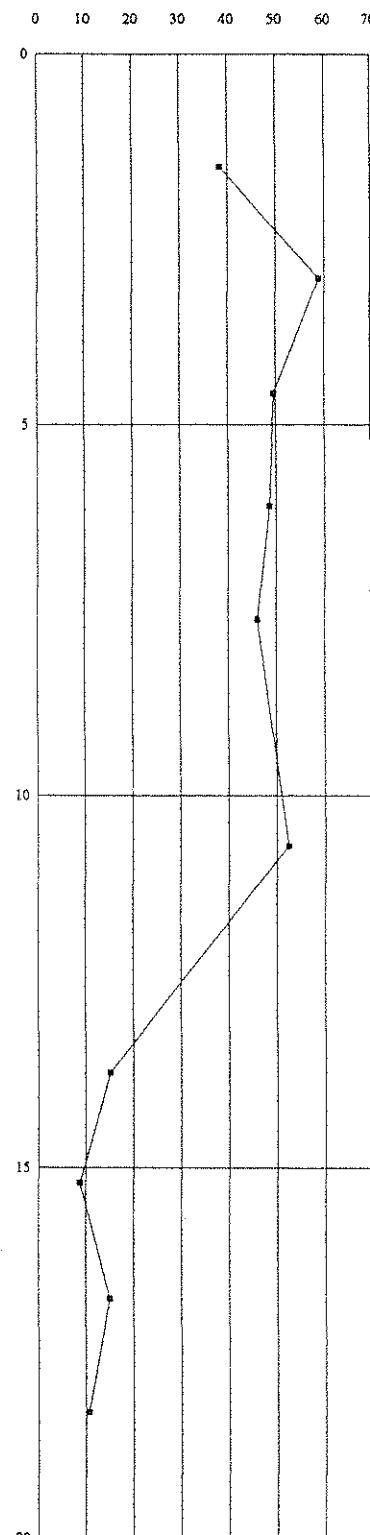
NOTES

END OF TEST HOLE AT 22.25 ON
PROBABLE BOULDERSHOLE OPEN TO 11.28 AT COMPLETION OF DRILLING
STANDPIPE 18.3 LONG WAS INSTALLED WITH
TIP AT 18.2 BELOW GRADE

DYREGROV CONSULTANTS		Logged/Drawn: SDG Checked: AOD	Test Hole No. 2007-16A	Project No. 272939
PROJECT: SEWPCC CLIENT: STANTEC CONSULTING LTD.			DATE OF INVEST : SEPTEMBER 17, 2007 DRILL : SUBTERRANEAN 125 mm AUGER	
SAMPLE NO.	DEPTH (M)	ELEV. (M)	S Y M	SOIL DESCRIPTION
				MOISTURE CONTENT (%)
				0 10 20 30 40 50 60 70
	0.00	231.92		O.00-0.15 TOPSOIL
	0.50	231.42		O.15-12.50 CLAY
	1.00	230.92		BROWN, SILTY, VERY STIFF TO STIFF
	1.50	230.42		HIGH PLASTIC
	2.00	229.92		MOTTLED BROWN
	2.50	229.42		TRACE SILT INCLUSIONS
	3.00	228.92		SILTY, STIFF
	3.50	228.42		HIGHLY PLASTIC
	4.00	227.92		MOTTLED BROWN
	4.50	227.42		GYPSUM INCLUSIONS
	5.00	226.92		TRACE SILT INCLUSIONS
	5.50	226.42		LAMINATION STRUCTURE
	6.00	225.92		
	6.50	225.42		
	7.00	224.92		
	7.50	224.42		
	8.00	223.92		GREY AT 7.93
	8.50	223.42		
	9.00	222.92		
	9.50	222.42		
	10.00	221.92		
	10.50	221.42		
	11.00	220.92		
	11.50	220.42		
	12.00	219.92		
	12.50	219.42		12.50-22.86 GLACIAL SILT TILL
	13.00	218.92		SILTY, SANDY, SOME GRAVEL
	13.50	218.42		TAN, LOOSE, SOFT
	14.00	217.92		COBBLES AND BOULDERS
	14.50	217.42		FEW CLAY SEAMS AND INCLUSIONS
	15.00	216.92		COBBLY AND BOULDERY, MORE DENSE BELOW
	15.50	216.42		13.7
	16.00	215.92		
	16.50	215.42		MORE SOFT AND LOOSE BELOW
	17.00	214.92		15.2
	17.50	214.42		
	18.00	213.92		
	18.50	213.42		HARDER DRILLING FROM 18.3 TO 19.8,
	19.00	212.92		BOULDERY, WATER ON AUGERS
	19.50	212.42		
	20.00	211.92		

NOTES

W/L DATE ELEV

Sept 18/07 221.1
Sept 19/07 223.46END OF TEST HOLE AT 22.86 AT
AUGER REFUSALPIEZOMETER INSTALLED TO 18.29 WITH
BOTTOM 3.05 SLOTTED

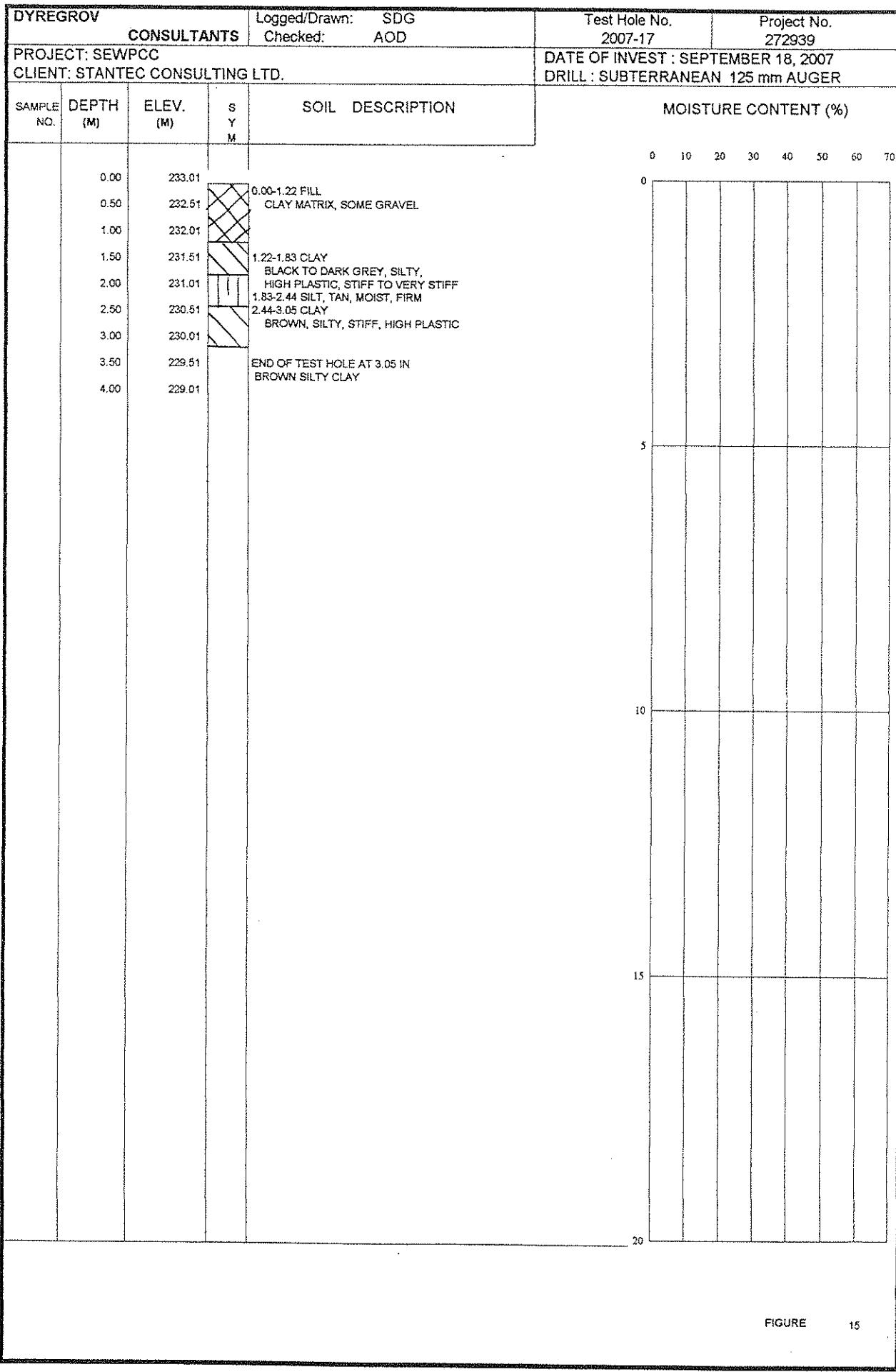


FIGURE 15

DYREGROV CONSULTANTS				Logged/Drawn: SDG Checked: AOD	Test Hole No. 2007-19	Project No. 272939	
PROJECT: SEWPCC CLIENT: STANTEC CONSULTING LTD.				DATE OF INVEST : SEPTEMBER 17, 2007 DRILL : SUBTERRANEAN 125 mm AUGER			
SAMPLE NO.	DEPTH (M)	ELEV. (M)	S Y M	SOIL DESCRIPTION	MOISTURE CONTENT (%)		
	0.00	231.77		0.00-0.15 TOPSOIL 0.15-3.05 CLAY SILTY, VERY STIFF TO STIFF HIGH PLASTIC, MOTTLED BROWN	0	10	20
	0.50	231.27			30	40	50
	1.00	230.77			60	70	
	1.50	230.27					
	2.00	229.77					
	2.50	229.27					
	3.00	228.77					
	3.50	228.27		END OF TEST HOLE AT 3.05 IN BROWN CLAY			
	4.00	227.77					

The figure is a soil profile diagram. The vertical axis on the left represents depth in meters, ranging from 0.00 at the top to 4.00 at the bottom. The horizontal axis at the top represents moisture content in percent, ranging from 0 to 70. A vertical line represents the soil profile. The topsoil layer (0-0.15m) is at 231.77m elevation. Below this is a clay layer (0.15-3.05m) described as silty, very stiff to stiff, high plastic, and mottled brown. A note states 'END OF TEST HOLE AT 3.05 IN BROWN CLAY'. The bottom part of the profile is at 227.77m elevation.

FIGURE 10

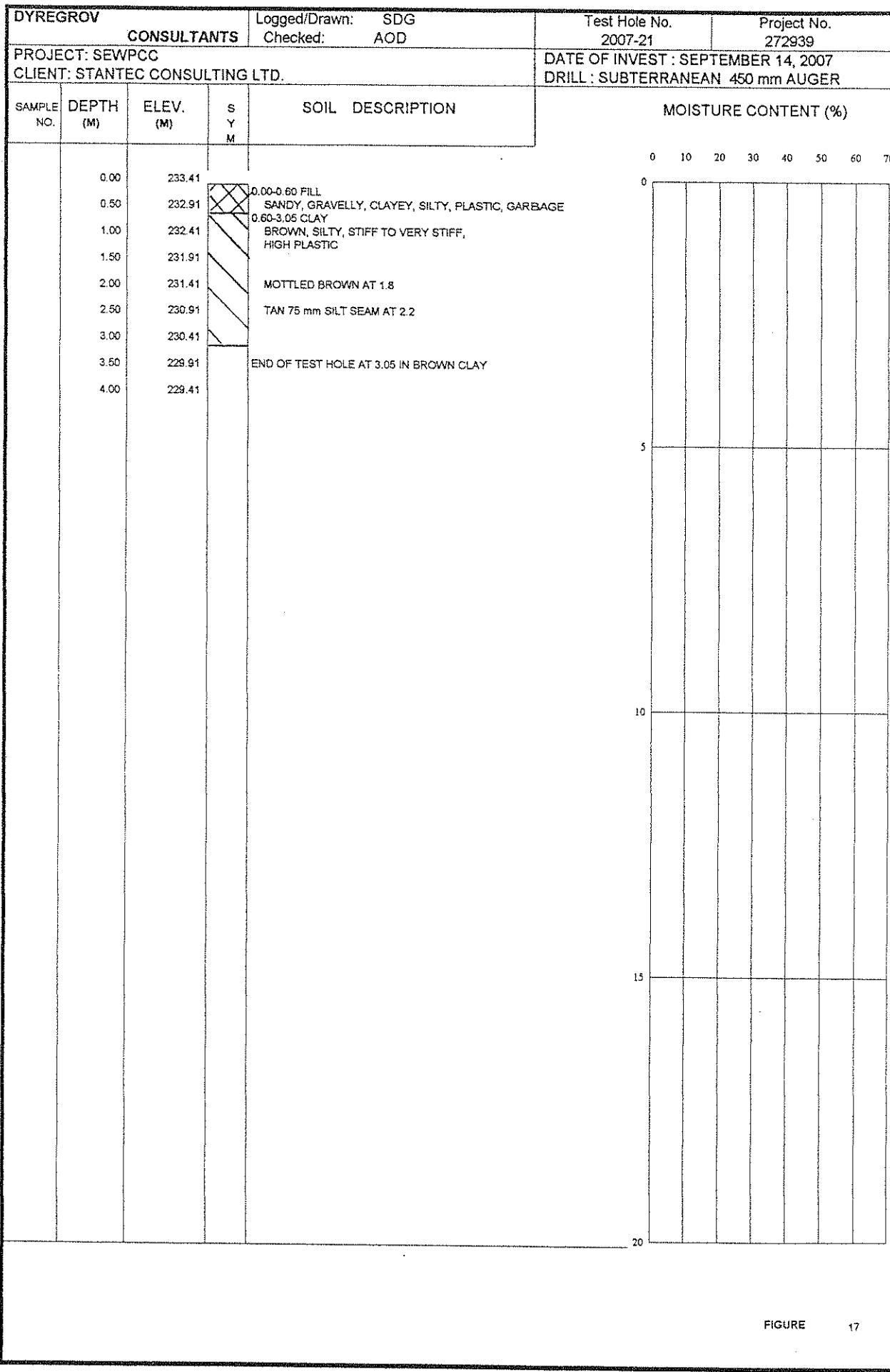
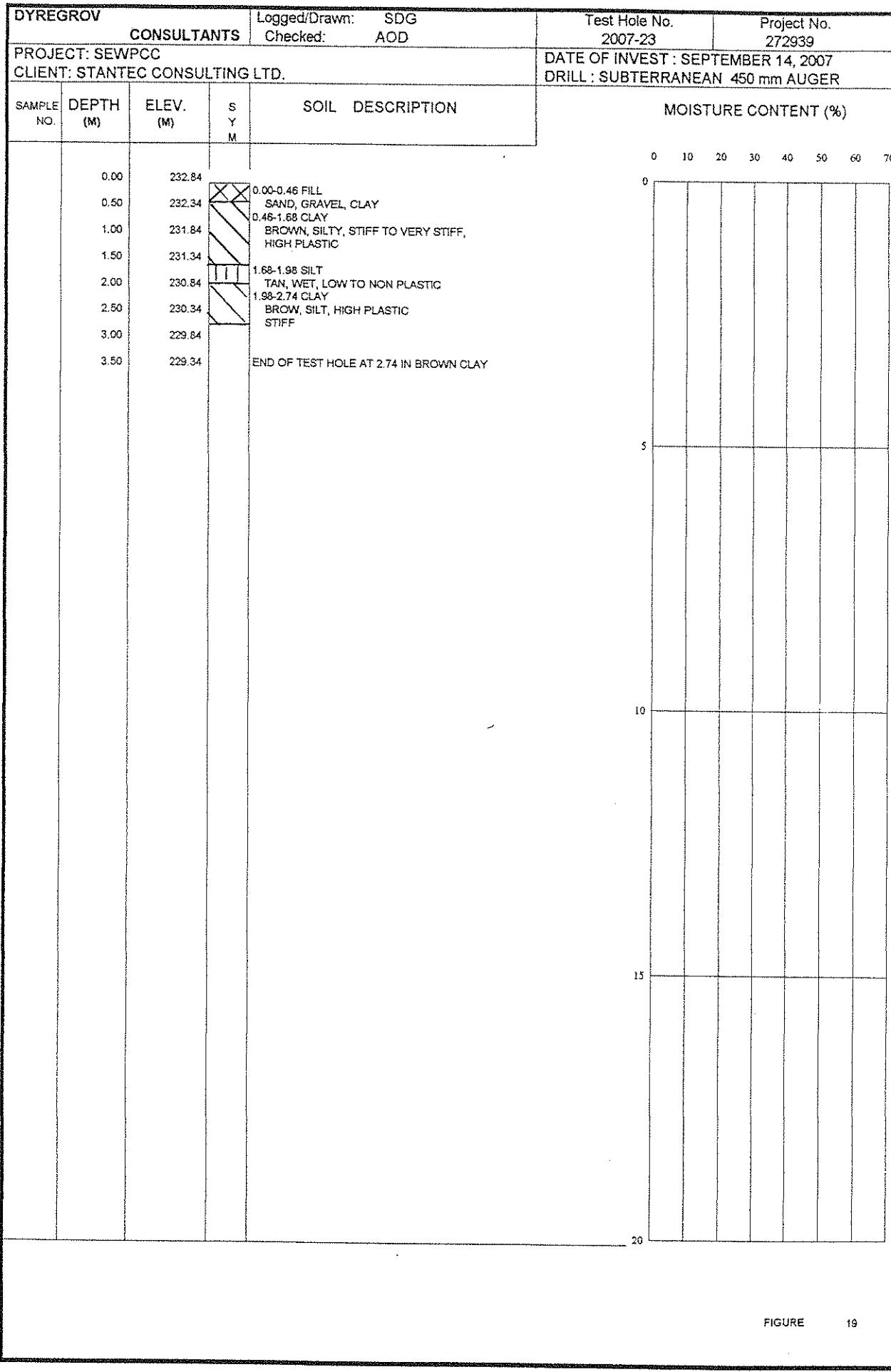


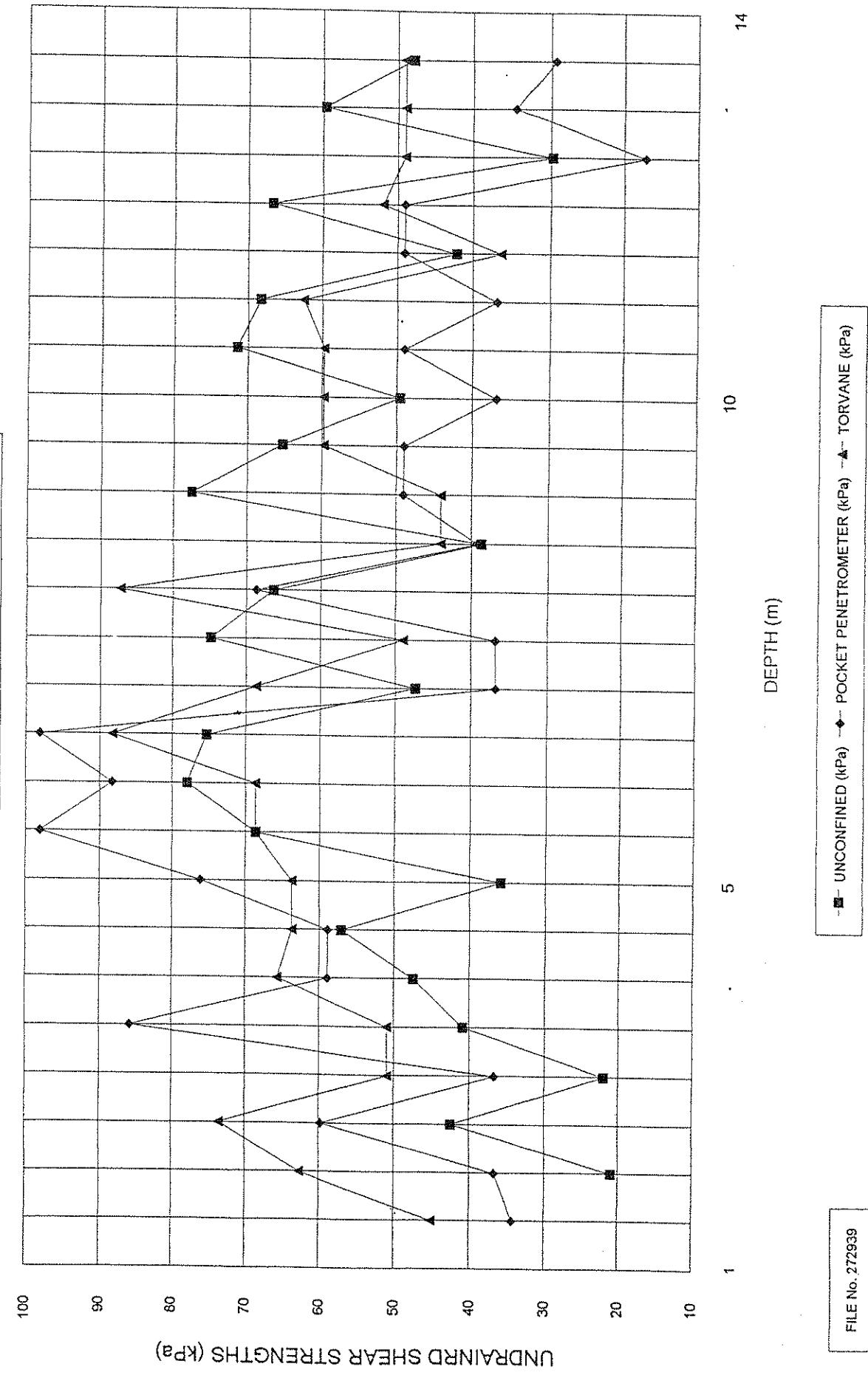
FIGURE 17

DYREGROV CONSULTANTS			Logged/Drawn: Checked:	SDG AOD	Test Hole No. 2007-22	Project No. 272939						
PROJECT: SEWPCC CLIENT: STANTEC CONSULTING LTD.					DATE OF INVEST : SEPTEMBER 14, 2007 DRILL : SUBTERRANEAN 450 mm AUGER							
SAMPLE NO.	DEPTH (M)	ELEV. (M)	S Y M	SOIL DESCRIPTION	MOISTURE CONTENT (%)							
					0	10	20	30	40	50	60	70
	0.00	232.51		0.00-0.38 FILL	0							
	0.50	232.01	X X X X	SAND, SOME GRAVEL, SILT								
				0.38-2.74 CLAY								
	1.00	231.51		BROWN, SILTY, STIFF TO VERY STIFF, HIGH PLASTIC								
	1.50	231.01		MOTTLED BROWN AT 1.5								
	2.00	230.51		50 TO 75 mm SILT LENSES BETWEEN 1.82 & 1.82								
	2.50	230.01										
	3.00	229.51										
	3.50	229.01		END OF TEST HOLE AT 2.74 IN BROWN CLAY								
					5							
					10							
					15							
					20							

FIGURE 18



SEWPCC
UNDRAINED SHEAR STRENGTHS vs DEPTH (M)



14

FIGURE 20

LOCATION: RIVER LOT 0153 IN PARISH OF St. Norbert

Owner: CITY OF WPG/WRB
Driller: M.R. HALL DRILLING LTD
Well Name: G05OC007 MO-16 SEWPCC
Well Use: OBSERVATION
Water Use:
UTMX: 637014
UTMY: 5517555
Accuracy XY: 1 EXACT [<5M] [GPS]
UTMZ: 233.629
Accuracy Z: 1 EXACT <10CM
Date Completed: 1971 Jan 01

WELL LOG

From (ft.)	To (ft.)	Log
0	5.0	DARK BROWN CLAY
5.0	6.0	SILTY BROWN CLAY
6.0	33.0	BROWN CLAY
33.0	47.0	GREY CLAY
47.0	55.0	SANDY STONY BROWN TILL
55.0	66.5	SILTY FINE SAND, COARSE GRAVEL STREAKS
66.5	71.0	LIMESTONE
71.0	72.0	SHATTERED LIMESTONE
72.0	76.0	LIMESTONE
76.0	77.0	SHATTERED LIMESTONE
77.0	81.9	LIMESTONE
81.9	82.9	SHATTERED LIMESTONE
82.9	99.9	LIMESTONE

WELL CONSTRUCTION

From (ft.)	To (ft.)	Casing Type	Inside Dia.(in)	Outside Dia.(in)	Slot Size(in)	Type	Material
0	67.8	casing	4.00			IRON	
67.8	99.9	open hole	4.00				

Top of Casing: 18.0 ft. below ground

No pump test data for this well.

REMARKS

SOUTH EAST WINNIPEG POLLUTION CONTROL CENTRE, TEST HOLE #3, WELL IN BASEMENT, SE CORNER, DOWN 4 FLIGHTS OF STAIRS, BOILER ROOM, CASING CEMENTED IN PLACE, E-LOGGED TO 98 FT, CHEMICAL ANALYSIS GROUND LEVEL ELEV MEASURED 233.629 M

FIGURE 21

G05OC007 SEWPCC MO-16 153 ST NORBERT
GROUND LEVEL ELEVATION 233.629 METRES (766.50 FEET)

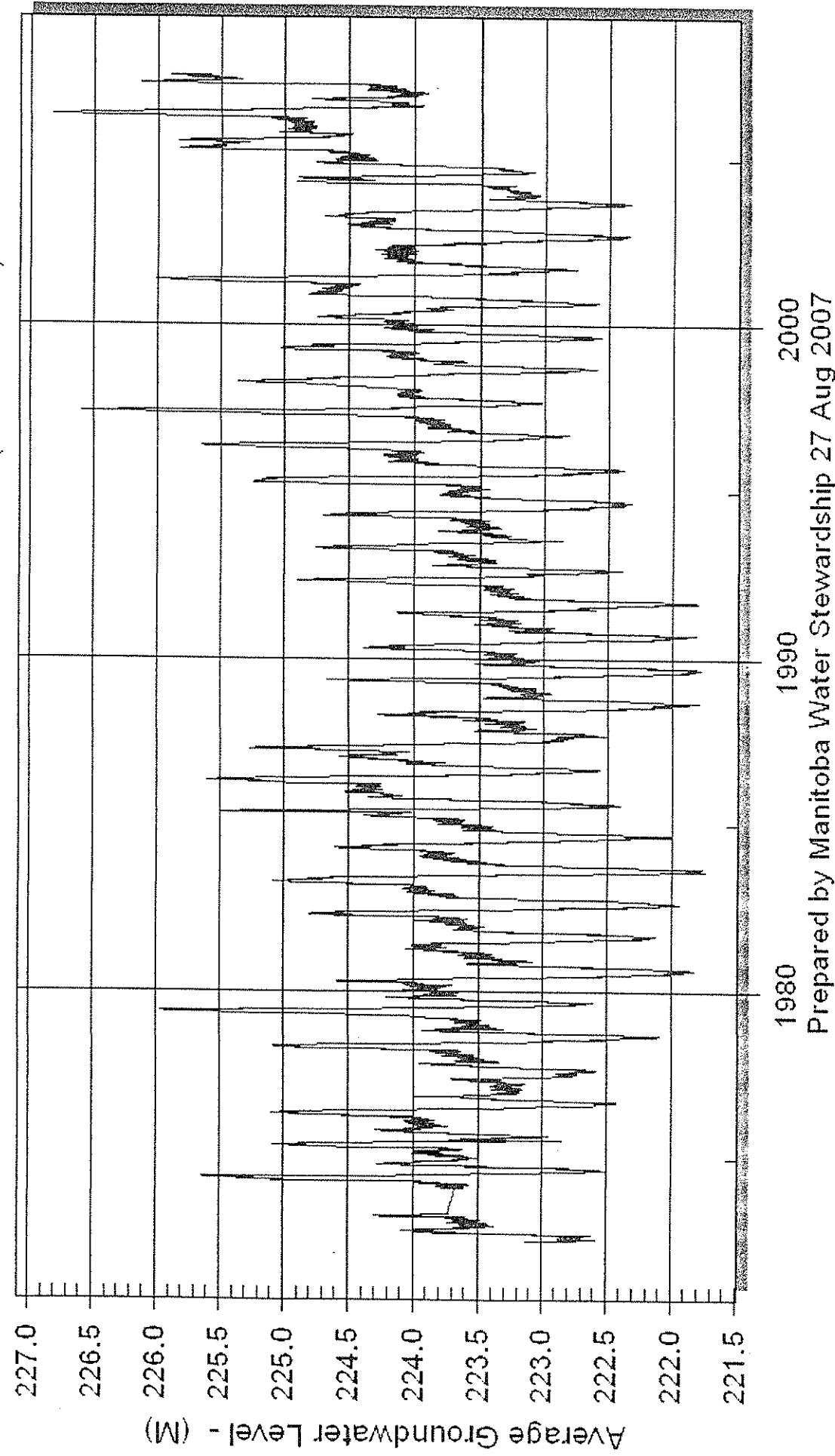
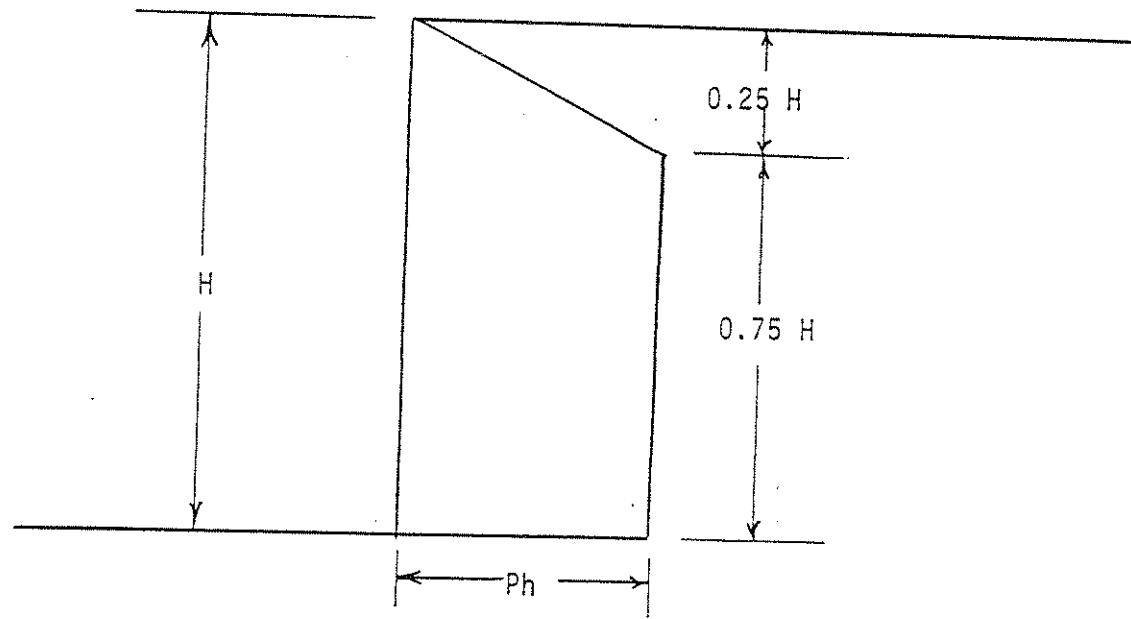


FIGURE 22



$$P_h = 0.4\gamma H$$

Where: P_h = Lateral earth pressure on shoring (kPa)

γ = Soil unit weight (17.28 kN/M³)

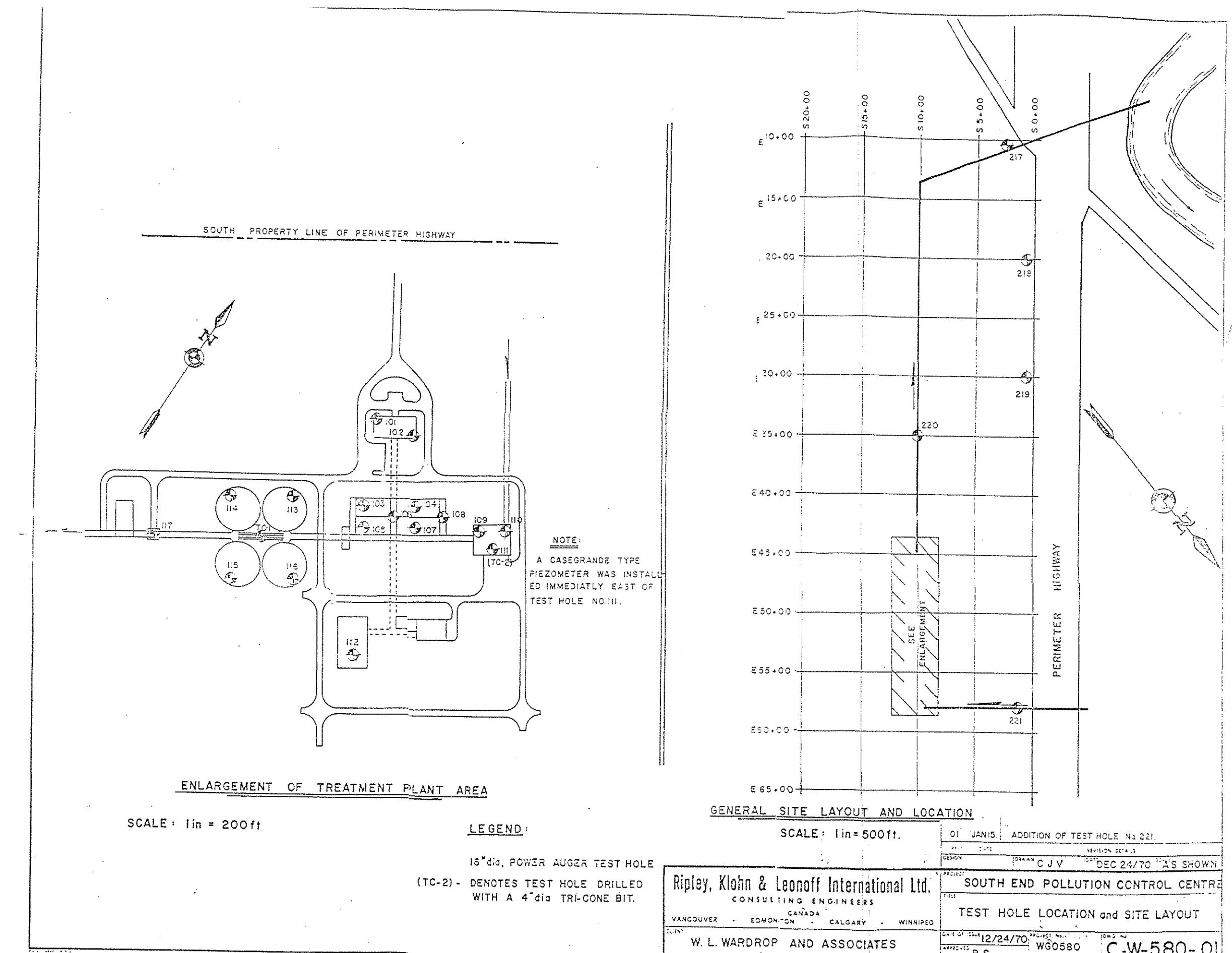
H = Wall height (M)

Note: Add surface load surcharge where applicable

APPENDIX

87528

TITLE: REPORT ON SUBSOIL INVESTIGATION
PROPOSED SOUTH END POLLUTION
CONTROL CENTRE
LOCATION: WINNIPEG, MANITOBA
CLIENT: METROPOLITAN CORPORATION OF
GREATER WINNIPEG
c/o W.L. WARDROP & ASSOCIATES
JOB NO: W-580 DATE: March 8, 1971



DATE November 12, 1970

TEST HOLE LOG

HOLE NO. 101



Ripley, Klohn & Leenoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

DISJECTA

SOUTH END POLLUTION CONTROL CENTRE

WINNIPEG, MANITOBA

TEST HOLE LOG

DATE December 1, 1970

HOLE NO. 102



Ripley, Klein & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

Project

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

DATE November 12, 1970

TEST HOLE LOG

HOLE NO. 103

SAMPLE DATA				ELEV. COLLAR	Unconfined Compression Tons Per Sq. Ft.			
WEIGHT HAMMER				ELEV. GROUND	1	2	3	4
HEIGHT DROP				CO-ORD. LOCATION	FIELD VANE	Δ LAB VANE	UNCONF.	
DEPTH ELEV.	G.D. IN.	BLOWS FT.	NO.	SYMBOL	PLASTIC LIMIT	WATER CONTENT	LIMIT LIQUID	
					X	—	—	X
10					10	30	50	70
13	2" Sy		2					90cc
15	Bag							
20	2" Sy		3					
25	Bag		5					
30	2" Sy		6					
35	Bag		7					
40	2" Sy		8					
45	Bag		9					
50			10					
52	Bag							
DESCRIPTION OF MATERIAL								
5	Bag	1		33	0.6'	TOPSOIL - black, highly organic		
10					4' to 5'	SILT LAYER - tan color - medium dense, - low plastic - moist		
13	2" Sy		2			CLAY - mottled brown & grey - highly plastic - layered structure - firm to stiff - moist - frequent small silt lumps and organic spots		
15	Bag							
20	2" Sy		3		18.5'			
25	Bag		5			CLAY - dark grey - highly plastic - layered structure - firm - moist - frequent small partings of silt & till-like material		
30	2" Sy		6			At 22' - inclusions of decayed organic		
35	Bag		7					
40	2" Sy		8					
45	Bag		9		42.5'	GLACIAL TILL - light grey - low to medium plastic clayey silt binder - stones to 2", soft, wet to saturated		
50			10					
52	Bag				52.5'	At 52.5' - becomes hard & moist		
NOTES								
<ol style="list-style-type: none"> 1. No water. 2. No sloughing of test hole. 3. Hole discontinued at 52.5 ft depth in glacial till. 								
<input type="checkbox"/> Pocket Penetrometer								



Ripley, Kohn & Leeser International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

DATE November 12, 1970

TEST HOLE LOG

HOLE NO.

104

SAMPLE DATA				SYMBOL	ELEV. COLLAR	Unconfined Compressive Tons Per Sq. Ft.				
DEPTH ELEV.	D.D. I.D.	BLOWS FT.	NO.		ELEV. GROUND	1	2	3	4	
					CO-ORD. LOCATION	• FIELD VANE Δ LAB VANE * UNCONFINED				
DEPTH ELEV.	D.D. I.D.	BLOWS FT.	NO.		DESCRIPTION OF MATERIAL	PLASTIC LIMIT	WATER CONTENT	L.C.		
5	Bag		1		TOPSOIL - black, highly organic	X	0	10	30	
10	2 ¹ /2 Sy		2		3' to 4' SILT LAYER - tan color; low plastic, clayey - wet, soft			50	70	
15	Bag		3		CLAY - mottled brown & grey - highly plastic - layered structure - firm, moist - occasional partings of silt and gypsum crystals					
20	2 ¹ /2 Sy		4							
25	Bag		5		CLAY - dark grey - highly plastic - soft to firm - damp - occasional partings of non-plastic silt & till-like material - some pebbles to $\frac{1}{4}$ "					
30	2 ¹ /2 Sy		6							
35	Bag		7							
40	2 ¹ /2 Sy		8							
47	Bag		9							
50					GLACIAL TILL - light grey color - low to medium plastic - clayey silt binder - soft, wet - stones to $1\frac{1}{2}$ "					
52	Bag		10							

NOTES

1. No water.
2. No sloughing of test hole.
3. Hole discontinued at 52.0 ft depth (maximum auger depth) in soft glacial till.

 Pocket Penetrometer

Ripley, Kohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

DATE December 12, 1970

TEST HOLE LOG

HOLE NO. 105

SAMPLE DATA				SYMBOL	ELEV. COLLAR	Unconfined Compression Tons Per Sq. Ft.						
WEIGHT HAMMER					ELEV. GROUND	1	2	3	4			
HEIGHT DROP					CO-ORD. LOCATION	FIELD VANE	LAB VANE	UNCONF.				
DEPTH ELEV.	G.D. IN.	BLOWS FT.	NO.		DESCRIPTION OF MATERIAL	PLASTIC LIMIT	WATER CONTENT	LIMIT LIQUID				
				{ } 1.0 TOPSOIL - black, highly organic								
5	2" Sy		1		CLAY - mottled brown & grey - highly plastic - layered structure - firm to stiff - moist - occasional partings of silt and of gypsum crystals							
10	Bag		2									
15	2" Sy		3									
20	Bag		4									
25	2" Sy		5		At 5' - numerous seams of tan silt							
30	Bag		6	30.0'								
35	2" Sy		7		CLAY - dark grey - highly plastic - layered structure - soft to firm - damp to wet - occasional small partings of silt & till-like material							
40	Bag		8									
45	2" Sy		9	42.5'	GLACIAL TILL - light grey color, - low to medium plastic clayey silt binder, soft, wet - pebbles to 3/4"							
50			10		At 47' to 48' - till is pinkish in color.							
52.5	Bag			52.5'	At 52' - till becomes hard, moist							
					NOTES							
					1. No water.							
					2. No sloughing of test hole.							
					3. Hole discontinued at 52.5 ft in hard Glacial Till.							
						<input checked="" type="checkbox"/> Pocket Penetrometer						



Ripley, Klehn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

DATE December 1, 1970

TEST HOLE LOG

HOLE NO. 106

SAMPLE DATA				ELEV. COLLAR	Unconfined Compression Tons Per Sq. Ft.			
WEIGHT HAMMER				ELEV. GROUND	1	2	3	4
HEIGHT DROP				CO-ORD. LOCATION	FIELD VANE	LAB VALUE	UNCONF.	
DEPTH ELEV.	D.D. I.D.	BLOWS FT.	NO.	DESCRIPTION OF MATERIAL	PLASTIC LIMIT	WATER CONTENT	LIQUID LIMIT	
				DESCRIPTION OF MATERIAL	X	— O —	— X —	10 30 50 70 90%
5	Bag	1	SS	1.0' TOPSOIL - black, highly organic				
10	2" Sy	2		1' to 3.5' SILT LAYER - tan, low plastic				
15	Bag	3		- medium dense				
20	2" Sy	4		- wet, soft,				
25	Bag	5		CLAY - mottled brown & grey				
				- highly plastic				
				- layered structure				
				- firm to stiff				
				- moist				
				From 20' - occasional partings of non-plastic silt.				
30	2" Sy	6		26.0'				
35	Bag	7		CLAY - dark grey				
40	2" Sy	8		- highly plastic				
45	Bag	9		- layered structure				
50		10		- soft to firm				
52	Bag			- moist to damp				
				At 40' - frequent partings of non-plastic silt and of till-like material				
				41.0'				
				GLACIAL TILL - light grey color				
				- medium plastic clayey silt binder, pebbles to 3/4"				
				- soft, wet				
				At 45' - inclusions of dark grey clay as above				
				52.0'				
				NOTES				
				1. No water.				
				2. No sloughing of test hole.				
				3. Hole discontinued at 52.0 ft depth in soft Glacial Till.				
					<input type="checkbox"/> Pocket Penetrometer			



Ripley, Kohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATION

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

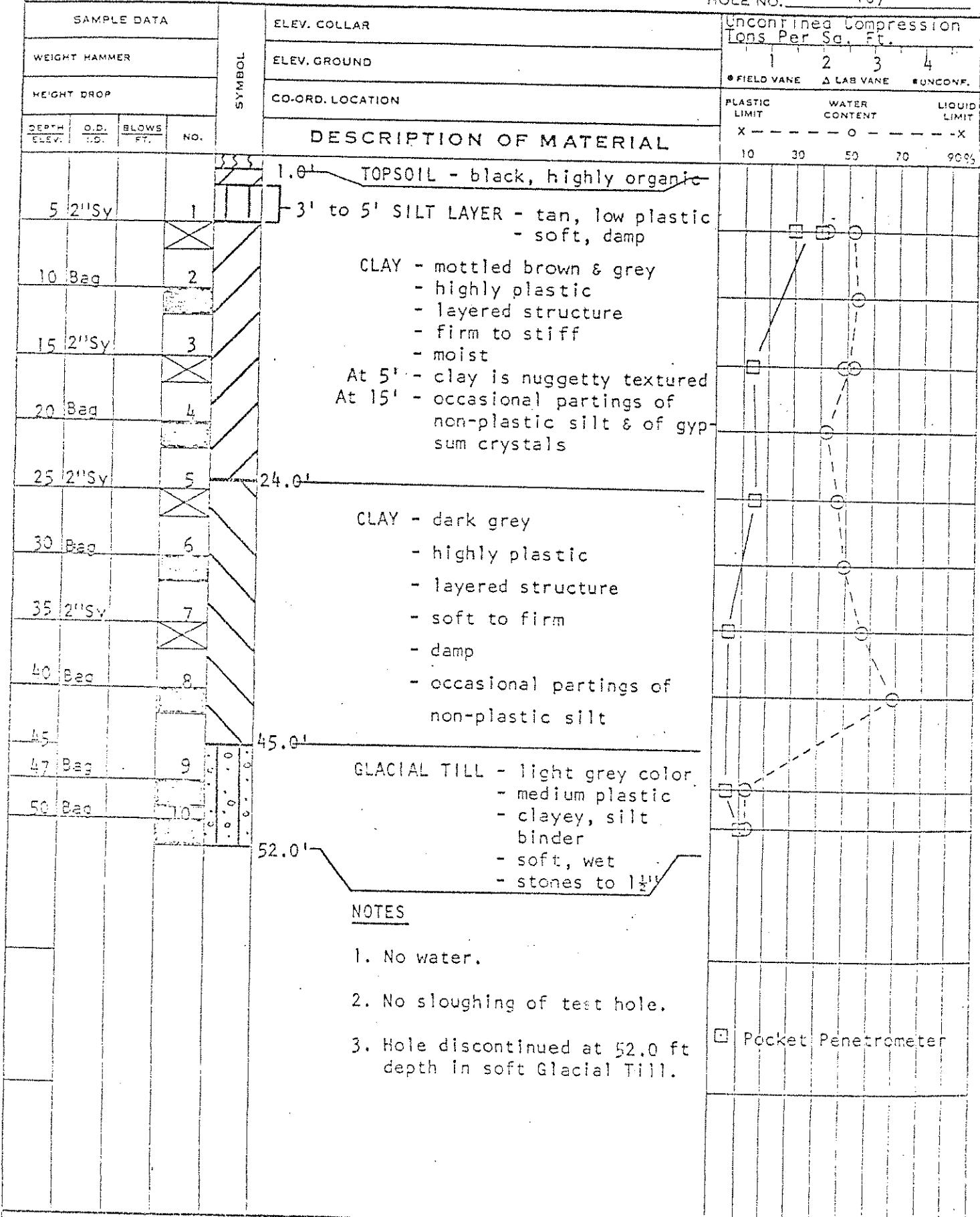
LOCATION

WINNIPEG, MANITOBA

DATE December 1, 1970

TEST HOLE LOG

HOLE NO. 107



Ripley, Kohn & Leonoff International Ltd.
CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE
LOCATION

WINNIPEG, MANITOBA

DATE December 1, 1970

TEST HOLE LOG

108

SAMPLE DATA				SYMBOL	ELEV. COLLAR	Unconfined Compression Tons Per Sq. Ft.				
WEIGHT HAMMER					ELEV. GROUND	1	2	3	4	
HEIGHT DROP					CO-ORD. LOCATION	FIELD VANE Δ LAB VANE *UNCONF.				
DEPTH ELEV.	O.D. I.D.	BLOWS FT.	NO.		DESCRIPTION OF MATERIAL	PLASTIC LIMIT	WATER CONTENT	Liquid Limit		
5	2' Sy	1			1.0' TOPSOIL - black, highly organic	X	0	-	-	
10	Bag	2			3' to 5' SILT LAYER - tan, low plastic. - soft, damp to wet	10	30	50	70	
15	2' Sy	3			CLAY - mottled brown & grey - highly plastic - layered structure - firm to stiff - moist - occasional partings of non plastic silt	1	1	1	1	
20	Bag	4			At 5' - clay has nuggety texture	2	2	2	2	
25	2' Sy	5			23.0' CLAY - dark grey - highly plastic - layered structure - firm - damp to wet	3	3	3	3	
30	Bag	6			- occasional partings of non-plastic silt & of till-like material	4	4	4	4	
35	2' Sy	7			44.0' GLACIAL TILL - light grey color. - medium plastic clayey silt binder - soft, wet - pebbles to 3/4"	5	5	5	5	
40	Bag	8				6	6	6	6	
45	2' Sy	9				7	7	7	7	
50	Bag	10				8	8	8	8	
					52.0' NOTES					
					1. No water.					
					2. No sloughing of test hole.					
					3. Hole discontinued at 52.0 ft depth in soft, wet, Glacial Till.					
									<input type="checkbox"/> Pocket Penetrometer	



Ripley, Kloha & Leonoff International Ltd.

CONSULTING ENGINEERS

卷之三 CHANGES IN SPUND 1710-1711

LIBRARY PROJECT

SOUTH END POLLUTION CONTROL CENTRE

WINNIPEG, MANITOBA

DATE December 2, 1970

TEST HOLE LOG

HOLE NO. 109

SAMPLE DATA				ELEV. COLLAR	RIG: Power Auger	Unconfined Compression Tons Per Sq. Ft.						
WEIGHT HAMMER				ELEV. GROUND	TECHNICIAN: J. Adams	1	2	3	4			
HEIGHT DROP				CO-ORD. LOCATION		FIELD VANE	△ LAB VANE	UNCONF.	LIMIT			
DEPTH ELEV.	O.D. I.D.	BLOWS FT.	NO.	DESCRIPTION OF MATERIAL								
						X	-	-	-	PLASTIC LIMIT	WATER CONTENT	LIQUID LIMIT
						10	30	50	70	90%		
5	2"SY		1		1.0'	TOPSOIL - black, highly organic						
						- 3' to 5' SILT LAYER - tan, low plastic						
						- soft, damp to wet						
10	Bag		2			CLAY - mottled brown & grey						
						- highly plastic						
15	2"SY		3			- layered structure						
						- firm to stiff						
20	Bag		4			- moist						
						- frequent small partings of						
25	2"SY		5		27.0'	non-plastic silt						
						CLAY - dark grey						
30	Bag		6			- highly plastic						
						- layered structure						
35	2"SY		7			- firm						
						- damp						
40	Bag		8			- numerous small partings of						
						non-plastic silt & of till						
45	Bag		9			like material						
					47.0'	GLACIAL TILL - light grey color						
50	Bag		10			- medium plastic						
					51.5'	- clayey silt						
						binder						
						- soft, wet						
<u>NOTES</u>												
1. No water.												
2. No sloughing of test hole.												
3. Refusal on boulder at 51.5 ft depth in soft Glacial Till.												
<input type="checkbox"/> Pocket Penetrometer												



Ripley, Kohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

DATE December 2, 1970

TEST HOLE LOG

HOLE NO. 110

SAMPLE DATA				SYMBOL	
WEIGHT HAMMER					
HEIGHT DROP					
DEPTH ELEV.	O.D. I.D.	BLOWS FT.	NO.		
5	Bad		1		
10	2 ¹ /2 Sy		2		
15	Bad		3		
20	2 ¹ /2 Sy		4		
25	Bad		5		
30	2 ¹ /2 Sy		6		
35	Bad		7		
40	2 ¹ /2 Sy		8		
45	Bad		9		
50	Bad		10		
52	Bad		11		

ELEV. COLLAR
ELEV. GROUND
CO-ORD. LOCATION

DESCRIPTION OF MATERIAL

1.0' TOPSOIL - black, highly organic
2' to 3' SILT LAYER - tan, low plastic
- soft, damp to wet

CLAY - mottled brown & grey
- highly plastic
- layered structure
- stiff
- moist
- frequent partings of non-plastic silt & gypsum crystals
At 21' - odd $\frac{1}{2}$ " silt seam, tan
- non-plastic

24.0'

CLAY - dark grey
- highly plastic
- layered structure
- firm
- damp
- frequent small partings of till-like material.

50.0'

GLACIAL TILL - light grey color
- medium plastic
clayey-silt binder, soft
- wet

NOTES

1. No water.
2. No sloughing of test hole.
3. Refusal on boulder at 52.0 ft depth in soft Glacial Till.

Unconfined Compression Tons Per Sq. Ft.			
1	2	3	4
• FIELD VANE	△ LAB VANE	■ UNCONFINED	
PLASTIC LIMIT	WATER CONTENT	LIMIT	
X	— O —	— X —	
10	30	50	70
			90%

 Pocket Penetrometer

Ripley, Klehn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT	SOUTH END POLLUTION CONTROL CENTRE		
LOCATION	WINNIPEG, MANITOBA		

DATE December 2, 1970

TEST HOLE LOG

HOLE NO. 111

SAMPLE DATA				ELEV. COLLAR	Unconfined Compression Tens Per Sq. Ft.
WEIGHT HAMMER				ELEV. GROUND	1 2 3 4
HEIGHT DROP				CO-ORD. LOCATION	• FIELD VANE Δ LAB VANE • UNCONS.
DEPTH ELEV.	O.D. IN.	BLOWS FT.	NO.	SYMBOL	PLASTIC LIMIT X-----O-----X 10 30 50 70 90%
DESCRIPTION OF MATERIAL					
5	2"	Sy	1	SS	1.0' TOPSOIL - black, highly organic
10	Bag		2		3.5' to 6' SILT LAYER - tan, low to non-plastic - soft, damp
15	2"	Sy	3		CLAY - mottled brown & grey - highly plastic - layered structure - firm to stiff - moist - frequent small partings of non-plastic silt and of gypsum crystals
20	Bag		4		
25	2"	Sy	5	25.0'	
30	Bag		6		
35	2"	Sy	7		CLAY - dark grey - highly plastic - layered structure - firm - moist to damp - frequent small partings of till-like material
40	Bag		8		
45	2"	Sy	9		
50	Bag		10		
52	Bag			51.0'	GLACIAL TILL
53	Bag				- light grey, medium plastic, clayey, silt At binder, soft, wet. 53' - becomes drier & dense
			11,12		
			13		
				53.0'	
NOTES					
<ol style="list-style-type: none"> 1. No water. 2. No sloughing of test hole. 3. Refusal at 53.0 ft depth on boulder in dense Glacial Till. 					
<input type="checkbox"/> Pocket Retetrometer					



Pippy, Kohn & Leonoff International Ltd.
CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT
SOUTH END POLLUTION CONTROL CENTRE
LOCATION
WINNIPEG, MANITOBA

DATE December 2, 1970

TEST HOLE LOG

HOLE NO. 112

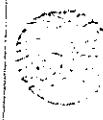
SAMPLE DATA

WEIGHT HAMMER				ELEV. COLLAR	Unconfined Compression Tons Per Sq. Ft.				
HEIGHT DROP				ELEV. GROUND	1	2	3	4	
DEPTH ELEV.	O.D. I.D.	BLOWS FT.	NO.	CO-ORD. LOCATION	• FIELD VANE	Δ LAB VANE	UNCONFINED		
				DESCRIPTION OF MATERIAL	PLASTIC LIMIT	WATER CONTENT	LIQUID LIMIT		
					X	— O —	— X —		
					10	30	50	70	90
5	Bag		1	1.0' TOPSOIL - black, highly organic					
10	2" Sy		2	CLAY - mottled brown & grey - highly plastic - layered structure - firm to stiff - moist - frequent small partings of non-plastic silt					
15	Bag		3						
20	2" Sy		4						
25	Bag		5						
30	2" Sy		6	27.0' CLAY - dark grey - highly plastic - layered structure - soft to firm - occasional small partings of non-plastic silt					
35	Bag		7	At 40' - numerous $\frac{1}{2}$ " seams of light grey Glacial Till pebbles to					
40	2" Sy		8						
45	Bag		9	41.0' GLACIAL TILL - light grey color - medium plastic, clayey-silt binder - soft, wet to saturated - pebbles to $3/4$ "					
50									

NOTES

1. No water.
2. Sloughing experienced in Glacial Till from 41.0 ft depth.
3. Hole discontinued at 47.0 ft depth in Glacial Till (due to drill failure).

Pocket Penetrometer



Ripley, Kohl & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTER

LOCATION

WINNIPEG MANITOBA

TEST HOLE LOG

DATE November 12, 1970

HOLE NO. 113

SAMPLE DATA				SYMBOL	ELEV. COLLAR	Unconfined Compression Tons Per Sq. Ft.							
WEIGHT HAMMER					ELEV. GROUND	1	2	3	4				
HEIGHT DROP					CO-ORD. LOCATION	FIELD VANE	LAB VANE	UNCONC.					
DEPTH ELEV.	O.D. I.D.	BLOWS FT.	NO.	DESCRIPTION OF MATERIAL									
10	2"	Sy	1		0.5'	TOPSOIL - black, highly organic							
15	Bag		2		1.0'	SILT - light grey	- moist						
20	2"	Sy	3			- loose, organic							
25	Bag		4		19.0'	CLAY - mottled brown & grey	- highly plastic						
30	2"	Sy	5			- layered structure	- firm to stiff						
35	Bag		6			- moist							
40	2"	Sy	7			- occasional small partings							
45	Bag		8			of gypsum							
50			9			From 1' to 7' - numerous seams							
52.5	Bag		10		47.0'	of very fine, tan, silty, sand, wet to sat.							
						CLAY - dark grey							
						- highly plastic							
						- layered structure							
						- soft to firm, damp							
						- frequent small partings							
						of till-like material							
						At 45' - traces of organic material							
						GLACIAL TILL							
						- light gray							
						- medium plastic, clayey							
						silt binder, soft,							
						wet to saturated							
						- pebbles to $\frac{1}{2}$ "							
						<u>NOTES</u>							
						1. Indication of water at 7.0 ft							
						and at 47.0 ft depths.							
						2. Some sloughing of sand layer(s)							
						at 7.0 ft depth.							
						3. Hole discontinued at 47.0 ft							
						depth in soft Glacial Till.							



Ripley, Kohn & Leonoff International Ltd.
CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE
LOCATION

WINNIPEG MANITOBA

Pocket Penetrometer

TEST HOLE LOG													
SAMPLE DATA				ELEV. COLLAR				HOLE NO. 114					
WEIGHT HAMMER				ELEV. GROUND				Unconfined Compression Tons Per Sq. Ft.					
HEIGHT DROP				CO-ORD. LOCATION				• FIELD VANE	△ LAB VANE				
DEPTH ELEV.	O.D. I.D.	BLOWS FT.	N.C.	DESCRIPTION OF MATERIAL				PLASTIC LIMIT	WATER CONTENT				
								X-----○-----X	LIQUEF LIMIT				
								10 30 50 70 90%					
				2.0' TOPSOIL - black, highly organic									
5	2" Sy	1		CLAY - mottled brown & grey - highly plastic - layered structure - firm to stiff, moist - frequent small partings of non-plastic silt & of gypsum crystal - rust stains & organic spots									
10	Bag	2		At 4' - 5' - layer(s) of tan silt									
15	2" Sy	3		26.0'									
20	Bag	4		CLAY - dark grey, highly plastic - layered structure - soft to firm - moist to damp - frequent small partings of till-like material									
25	2" Sy	5		30'									
30	Bag	6		35'									
35	2" Sy	7		40'									
40	Bag	8		45'									
45	2" Sy	9		GLACIAL TILL - light grey, medium plastic, clayey silt binder - soft, wet to saturated									
50	Bag	10		At 46' - becomes drier & quite dense									
				50.0'									
<u>NOTES</u>													
1. No water.													
2. No sloughing of test hole.													
3. Refusal at 50.0 ft depth on boulders on dense Glacial Till.													
<input type="checkbox"/> Pocket Penetrometer													



Ripley, Motil & Le Jeoff International Ltd.

CONSULTING ENGINEERS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

DATE December 18, 1970

TEST HOLE LOG

HOLE NO.

151



Ripley, Klohn & Leonoff International Ltd.

CONSULTING ENGINEERS | DR. MCGOWAN LTD.

RECORDED IN THE OFFICE OF THE CLERK OF THE COURT

SOUTH END POLLUTION CONTROL CENTRE

WINNIPEG, MANITOBA

DATE December 18, 1970

TEST HOLE LOG

HOLE NO. 116



Ripley, Kohn & Leonoff International Ltd.

CONSULTING ENGINEERS

BOB NECHI 80 + SOUNDALIVE

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

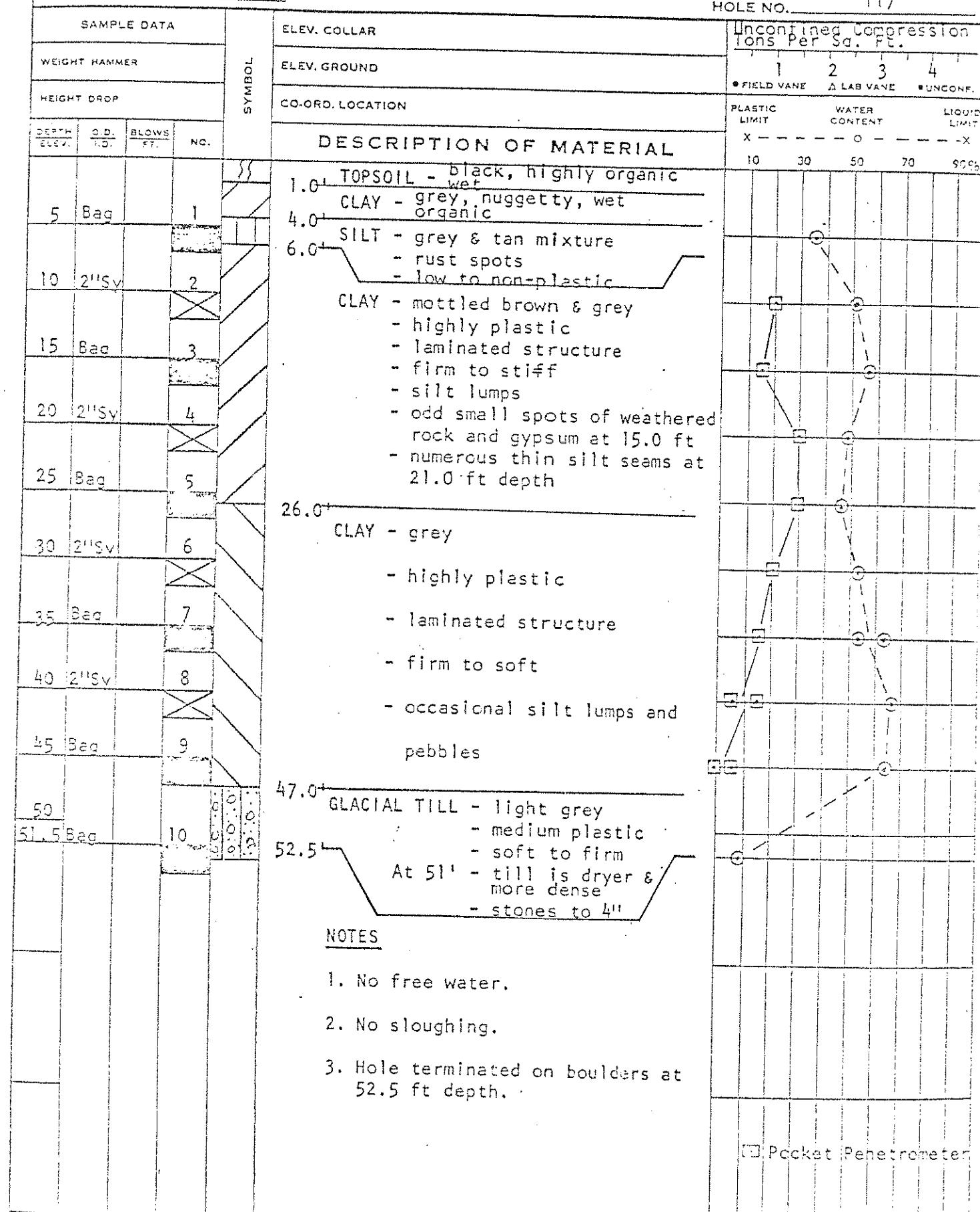
LOCATION

WINNIPEG, MANITOBA

DATE December 18, 1970

TEST HOLE LOG

HOLE NO. 117



Ripley, Kohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

DATE December 9, 1970

TEST HOLE LOG

HOLE NO. 217



Ripley, Klohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

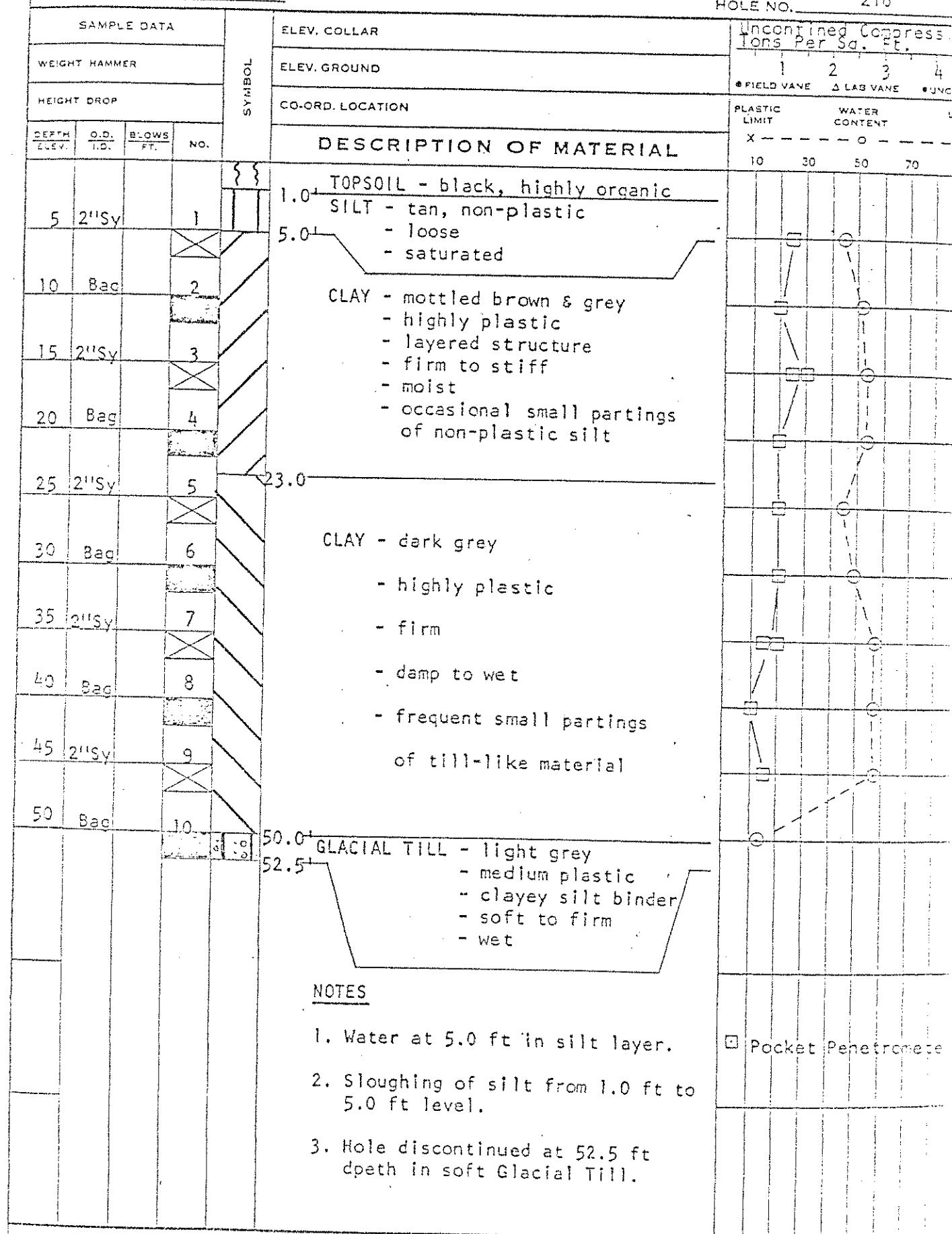
WINNIPEG, MANITOBA

DATE December 13, 1970

TEST HOLE LOG

HOLE NO.

218



Ripley, Kohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CEN

LOCATION

WINNIPEG, MANITOBA

TEST HOLE LOG

DATE December 21, 1970

HOLE NO. 219



Ripley, Kohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

DATE December 8, 1970

TEST HOLE LOG

HOLE NO. 220



Ripley, Klohn & Leonoff International Ltd.

CONSULTING ENGINEERS | **SOIL MECHANICS & FOUNDATIONS**

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

EDUCATION

WINNIPEG, MANITOBA

TEST HOLE LOG

DATE, January 15, 1971

HOLE NO. 221

SAMPLE DATA				SYMBOL	ELEV. COLLAR	Unconfined Compression Tons Per Sq. Ft.				
WEIGHT HAMMER					ELEV. GROUND	1	2	3	4	
HEIGHT DROP					CO-ORD. LOCATION	FIELD VANE	Δ LAR VANE	UNCONF.		
DEPTH CLEVI.	O.D. I.D.	BLOWS FT.	NO.		DESCRIPTION OF MATERIAL	PLASTIC LIMIT	WATER CONTENT	LIQUID LIMIT	X-----O-----X	
5	Bag	1	55		1.0' TOPSOIL - black, highly organic				10 30 50 70 90	
10	3"SY	2			7'-9' SILT - tan, medium dense, damp					
15	Bag	3			CLAY - mottled brown & grey - highly plastic - layered structure - firm to stiff - moist					
20	3"SY	4			At .18' - partings of white gypsum crystals					
25	Bag	5			23.0' CLAY - dark grey, - highly plastic - layered structure - soft to firm - damp to wet					
30	3"SY	6			- numerous small partings of light grey till-like material					
35	Bag	7			- frequent silt lumps to 1/2 inch					
40	3"SY	8								
45	Bag	9			45.0' NOTES					
					1. Hole discontinued at 45.0 ft. depth in grey clay.					
					2. No water. No sloughing.					
						<input type="checkbox"/> Pocket Penetrometer				

Ripley, Klohn & Leonoff International Ltd.

CONSULTING ENGINEERS | ARCHITECTS & PLANNERS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

DATE December 24, 1970

TEST HOLE LOG

HOLE NO. T.C. I

SAMPLE DATA			ELEV. COLLAR	RIG: Acker	COHESION - TONS/SQ. FT.					
WEIGHT HAMMER			ELEV. GROUND	TECHNICIAN: J. Adams	0.2	0.6	1.0	1.4	1.8	
WEIGHT DROP			CO-CRD. LOCATION		• FIELD VANE	△ LAB VANE	* UNCONF.			
DEPTH ELEV.	C.D. I.D.	BLOWS FT.	NO.	DESCRIPTION OF MATERIAL						
40				OVERBURDEN						
50				49.0' - TILL-LIKE - till						
60				- light grey						
70				- soft						
80				60.0' - TILL-LIKE - light grey						
				- firmer than above						
				65.0' - GLACIAL TILL - light grey						
				- hard						
				- cuttings were mostly light grey fine sands						
				74.0' - LIMESTONE - 74' to 77' very solid						
				- 77' to 79' softer lime stone, loss of water from pump						
				81.0' - 79'-81' - very solid lime-stone						
				<u>NOTES</u>						
				1. Auger refusal at 65.0 ft depth						
				2. Triccone used 65.0 - 81.0 ft depth.						
				3. Complete water loss below 77 ft depth.						



Ripley, Klein & Leonoff International Ltd.

CONSULTING ENGINEERS

SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

TEST HOLE LOG

DATE December 24, 1970

HOLE NO. T.C. 2

SAMPLE DATA				SYMBOL	ELEV. COLLAR	RIG: Acker	COHESION - TONS/SQ. FT.					
WEIGHT HAMMER					ELEV. GROUND	TECHNICIAN: J. Adams	0.2	0.6	1.0	1.4	1.8	
WEIGHT DROP					CO-ORD. LOCATION	• FIELD VANE △ LAB VANE □ UNCONF.						
DEPTH FT.	D. I.D.	BLOWS FT.	NO.		DESCRIPTION OF MATERIAL	PLASTIC LIMIT	WATER CONTENT	LIMIT LIQUID	X	-	-X	
						10	30	50	70		90%	
40					OVERBURDEN - See Test Bore #111							
50					50.0'							
60					TILL-LIKE	- light grey - soft - auger refusal at 60.5'						
70					60.5'	LIMESTONE - - 60.5' to 62.0' solid limestone - 62.0' to 63.0' layer of softer broken limestone						
					68.0'	- 63.0' to 63.5' solid limestone - 63.5' to 65.0' broken lime- stone - 65.0' to 68.0' solid lime- stone						
					NOTES							
					1. Water circulated into hole was lost.							
					2. End of hole. At 68.0 ft was in limestone.							



Ripley, Kohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

87003435

TITLE: REPORT ON INSTALLATION OF TEST
CAISSENS AT SOUTH END POLLUTION
CONTROL CENTRE T.P.
LOCATION: WINNIPEG, MANITOBA
CLIENT: W. L. WARDROP & ASSOCIATES LTD.
JOB NO: W - 619 DATE: March 24, 1971

**PROPERTY
OF THE
Waterworks, Waste & Disposal Department
MAIN OFFICE
RESOURCE CENTRE**

DATE March 4, 1971

TEST HOLE LOG

HOLE NO. Test Calsson #1

SAMPLE DATA				SYMBOL	ELEV. COLLAR	TECH: J. Odermatt	Unconfined Compression Tons Per Sq. Ft.						
WEIGHT HAMMER					ELEV. GROUND	RIG: Williams Auger	1	2	3	4			
HEIGHT DROP					CO-ORD. LOCATION	8+20S & 57+88E	• FIELD VANE	△ L.O. VANE	■ UNCONF.				
DEPTH ELEV.	O.D. I.D.	BLOWS FT.	NO.		DESCRIPTION OF MATERIAL								
10					CLAY - mottled brown & grey								
20					- highly plastic								
30					- layered structure								
40					25.0'								
50	Bag			1	CLAY - grey								
55	Bag			2	- highly plastic								
60	Bag			3	- layered structure								
65	Bag			4	47.5' TILL-LIKE MATERIAL								
70	Bag			5	- light grey, very sandy - silt binder - soft & wet, clayey - some cobbles & some sand layers or pockets								
					57.0' GLACIAL TILL - light tan								
					- very sandy dilates - soft cobbles - very little silt binder								
					60.0' GRAVEL - sandy with angular broken limestone (less than 18 inches dia.)								
					66.0' LIMESTONE - hard, broken - fractured, sand & gravel inclusions								
					67.5' LIMESTONE - hard, sound rock - competent rock								
					71.0' <input checked="" type="checkbox"/> Pocket Penetrometer <input checked="" type="checkbox"/> Disturbed Sample								



Ripley, Klohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

TEST HOLE LOG

DATE 5-19 271

HOLE NO. Test Caisson #1



Ripley, Klohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

TEST HOLE LOG

DATE March 5, 1971

HOLE NO. Test Caisson #2



Ripley, Klohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT
SOUTH END POLLUTION CONTROL CENT

LOCATION

WINNIPEG, MANITOBA

DATE March 5, 1971

TEST HOLE LOG

Test Caisson #2



Ripley, Klohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

PROJECT

SOUTH END POLLUTION CONTROL CENTRE

LOCATION

WINNIPEG, MANITOBA

REPO 711.246 1971

1963736

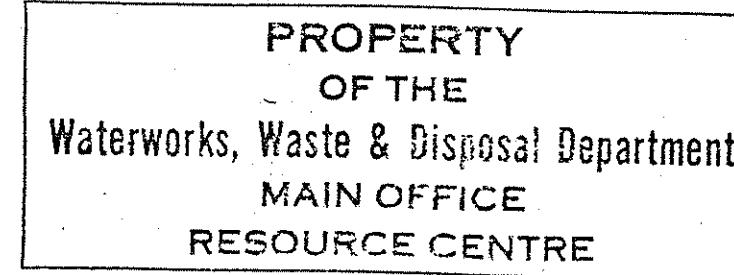
87003436

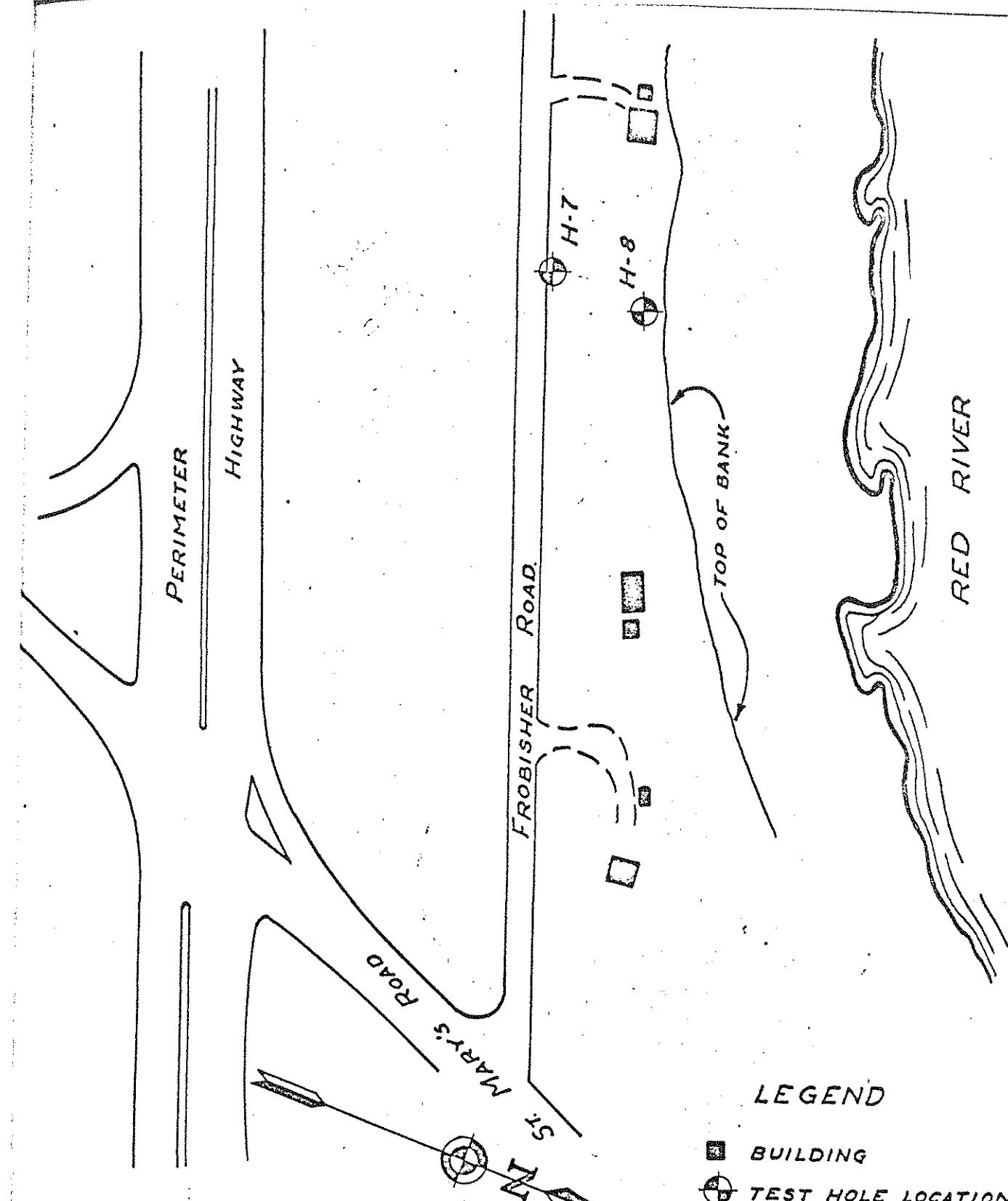
TITLE: TEST HOLES DRILLED AT OUTFALL
STAGE ASSOCIATED WITH SOUTH END
POLLUTION CONTROL CENTRE

LOCATION: WINNIPEG, MANITOBA

CLIENT: METRO WATERWORKS & WASTE DIS-
POSAL DIVISION

JOB NO: W-623 DATE: April 14, 1971





LEGEND

- BUILDING
- TEST HOLE LOCATION

SCALE 1"=100'

pley, Kohn & Leonoff International Ltd.
CONSULTING ENGINEERS
VANCOUVER — EDMONTON — CALGARY — WINNIPEG
CANADA
ENT.
M.C.G.W.

SUBSOIL INVESTIGATION
SEWAGE OUTFALL LOCATION
TEST-HOLE LOCATION PLAN.

APPROVED

R.S.

DATE 23/03/71 A-W-623-01

DATE March 24, 1971

TEST HOLE LOG

HOLE NO. 1

SAMPLE DATA				ELEV. COLLAR	TECH: C. J. Vann	Unconfined Compression Tons Per Sq. Ft.						
				ELEV. GROUND (759.9)	RIG: 16" Power Auger	1	2	3	4			
DEPTH ELEV.	O.D. I.D.	BLOWS FT.	NO.	CO-ORD. LOCATION				FIELD VANE	LAO VANE	UNCONF.		
				DESCRIPTION OF MATERIAL				PLASTIC LIMIT	WATER CONTENT	LIQUID LIMIT		
								X	- - - O - - - X			
								10	30	50	70	90%
10					CLAY - dark brown - sandy, silty - frequent inclusions of gypsum crystals	7.0'						
20					CLAY - mottled brown & grey - highly plastic - laminated structure - gypsum crystals - silt lumps - firm to stiff	24.0'						
30					CLAY - grey - highly plastic - laminated structure - silt lumps	31' Sy						
40					- at 45'0" - numerous till- like inclusions and material is wet and soft	31' Sy						
50					TILL-LIKE - light tan-grey - clayey, silt binder - firm - damp to wet, cobbles from 54'0"	31' Sy						
60					NOTES	50.0'						
					1. Water at 50'0" in till. 2. Hole discontinued at 60'0", the maximum extent of the auger.	60.0'						
							<input type="checkbox"/> Pocket Penetrometer					
								<input type="checkbox"/> Undisturbed Sample				



Ripley, Klohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

SEWAGE OUTFALL
SOUTH END POLLUTION CONTROL CENTRE

LOCATION

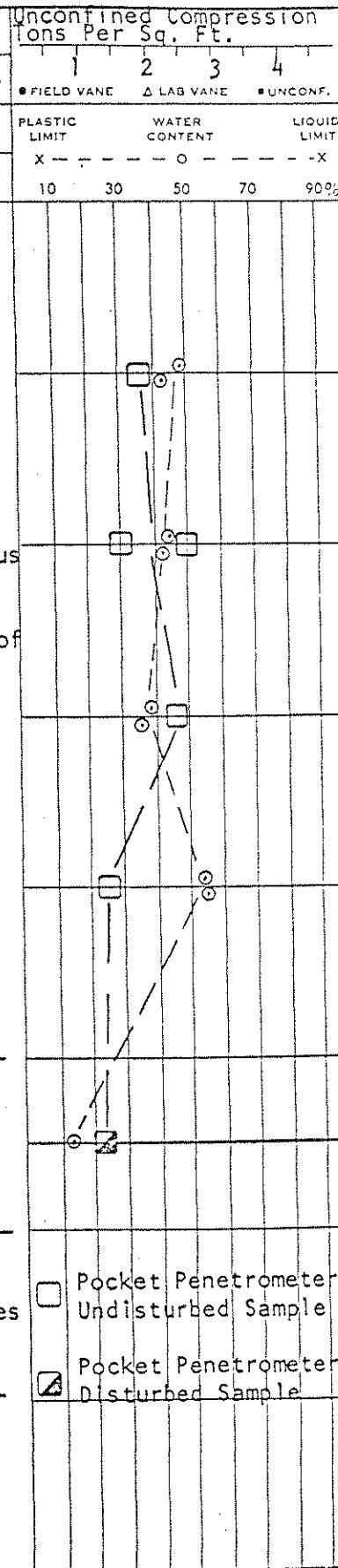
WINNIPEG MANITOBA

DATE March 24, 1971

TEST HOLE LOG

HOLE NO. 2

SAMPLE DATA				SYMBOL	ELEV. COLLAR	TECH: C. J. Vann	Unconfined Compression Tons Per Sq. Ft.				
WEIGHT HAMMER					ELEV. GROUND (758.8)	RIG: 16" Power Auger	1	2	3	4	
HEIGHT DROP					CO-ORD. LOCATION		• FIELD VANE	△ LAB VANE	■ UNCONF.		
DEPTH ELEV.	O.D. I.D.	BLOWS FT.	NO.		DESCRIPTION OF MATERIAL		PLASTIC LIMIT	WATER CONTENT	LIQUID LIMIT		
					CLAY - dark brown, sandy, silty - moist - firm to stiff		X	-	-		
					6'0"		10	30	50		
10	3"Sy		1		CLAY - mottled brown & grey. - highly plastic - laminated structure - gypsum inclusions at 10'0" - silt lumps - from 6'0" to 8'0" - numerous layers of tan silt - at 17'0" to 19'0" - layer of grey clay		70	90%	-X		
20	3"Sy		2		30.0'						
30	3"Sy		3		CLAY - grey, highly plastic - laminated structure - silt lumps, firm to stiff - at 35'0" - frequent in- clusions of till-like material, at 46'0" - large seams of soft till-like material						
40	3"Sy		4		50.0'						
50	Bag		5		TILL-LIKE - light tan-grey - soft, damp to wet - cobbles & boulders from 55'0"						
60					NOTES						
					1. Water at 50'0", fifteen minutes after drilling.						
					2. Hole ended at 60'0", the maxi- mum depth of the auger.						



Ripley, Klohn & Leonoff International Ltd.

CONSULTING ENGINEERS | SOIL MECHANICS & FOUNDATIONS

SEWAGE OUTFALL
SOUTH END POLLUTION CONTROL CENTRE
LOCATION WINNIPEG, MANITOBA

GEOTECHNICAL ENGINEERING REPORT

SOUTH END WATER POLLUTION CONTROL CENTRE

Prepared For

WARDROP ENGINEERING INC.

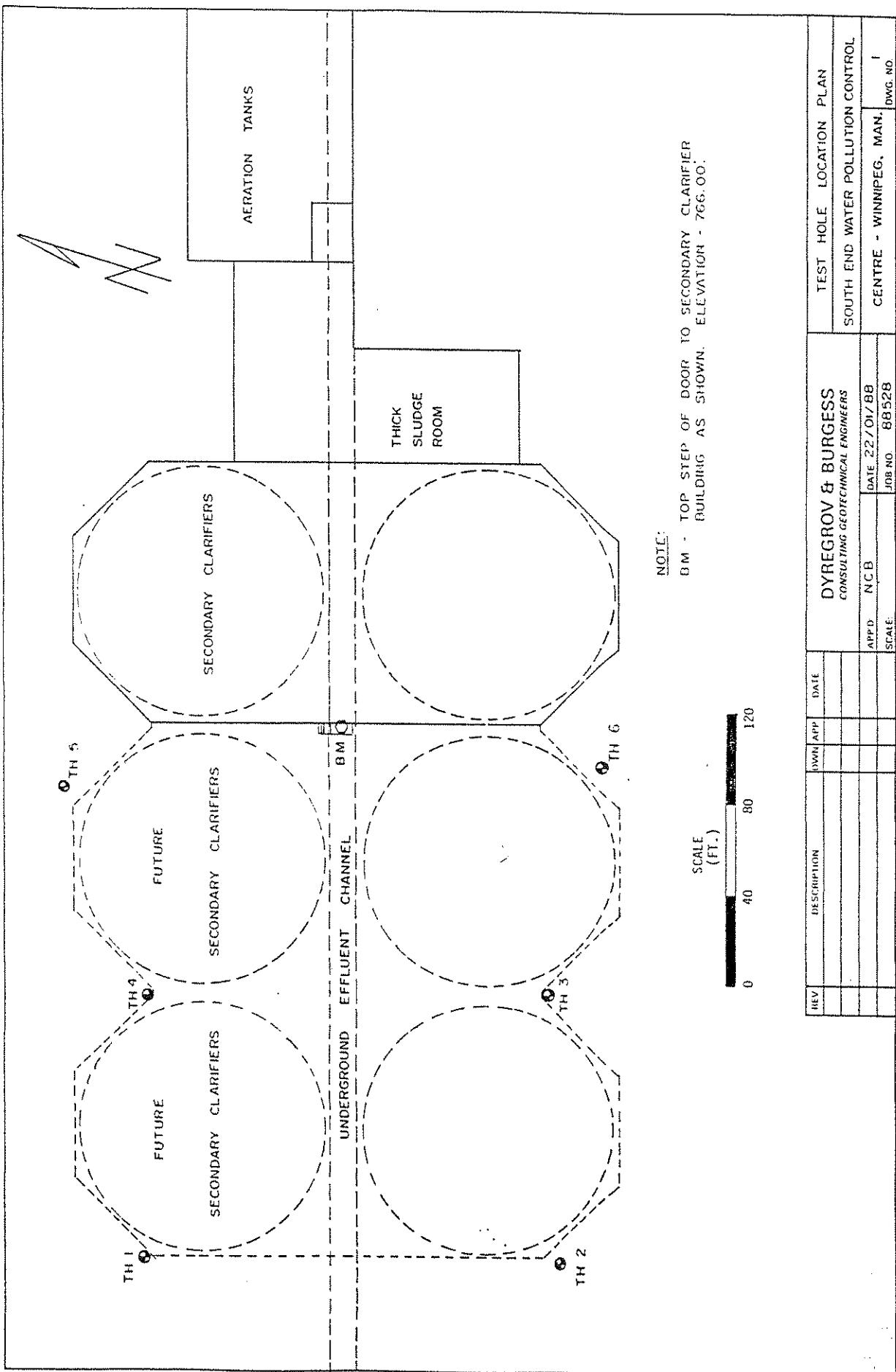
MACLAREN ENGINEERS INC.

On Behalf of

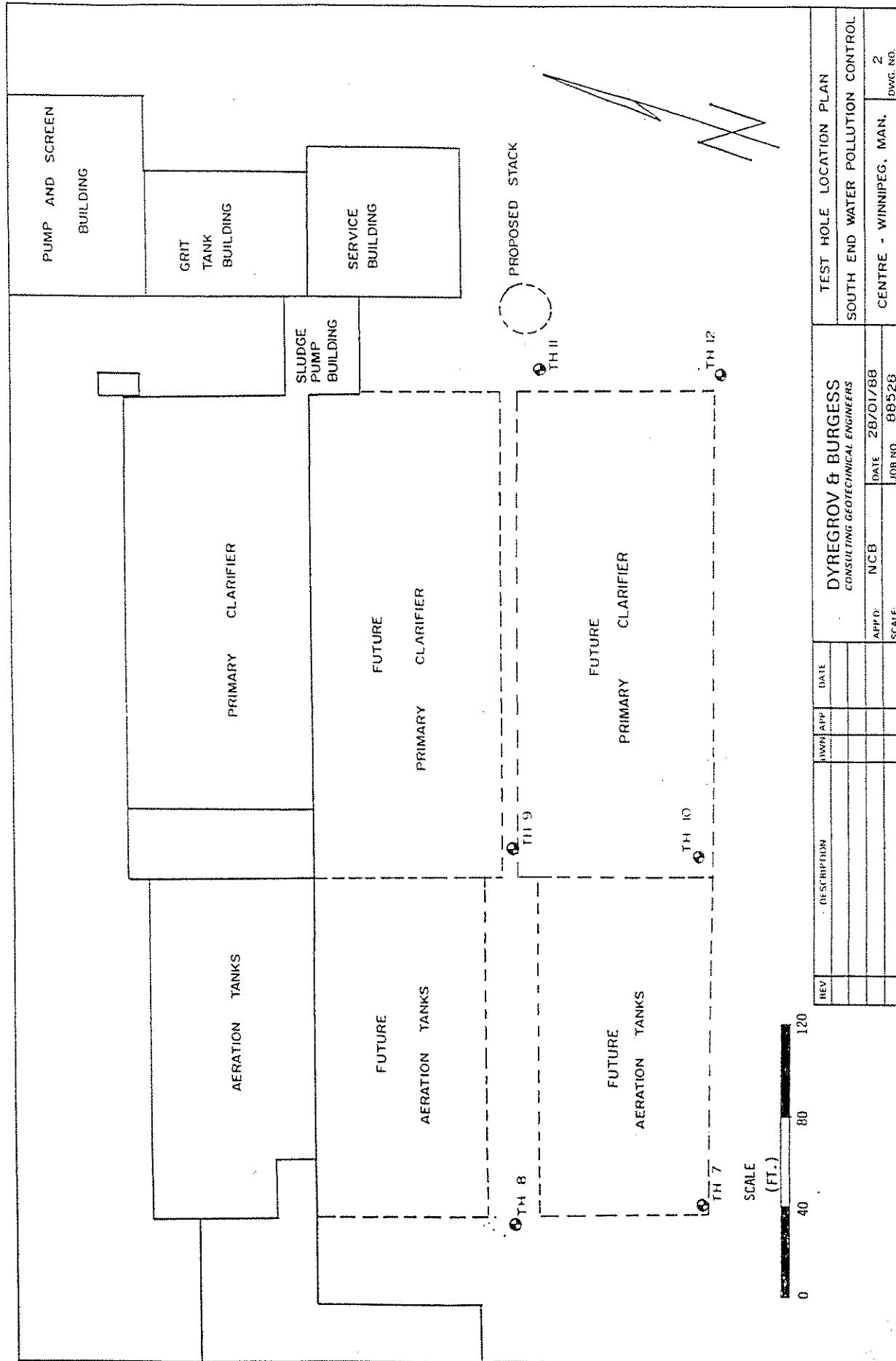
THE CITY OF WINNIPEG

April 15, 1988

Project No. 88528



REV	DESCRIPTION	OWN APP	DATE	DYREGROV & BURGESS CONSULTING GEOTECHNICAL ENGINEERS	TEST HOLE LOCATION PLAN
				APPD N.C.B	SOUTH END WATER POLLUTION CONTROL
				DATE 22/OV/98	CENTRE - WINNIPEG, MAN,
				JOB NO 88528	! DWG. NO.
				SCALE	



DYREGROV & BURGESS

BOREHOLE LOG

PROJECT

South End Water Pollution Control Centre

LOGGED/DWN:	SDG	CXD.	NCR	DATE OF INVEST.	29/02/88	JOB NO.	88528	HOLE NO.
				SOIL DESCRIPTION		SOIL SAMPLE		DRILL TYPE
				DATUM		CONDITION	TYPE	PENETRATION RESISTANCE
				SURFACE ELEVATION 762.17'				
W _p - □	w - ○	w _L - △		DEPTH (FT)	SOIL SYMBOL			
PERCENT %	10 20 30 40 50 60			0	X	Fill -clay, trace gravel		
						Clay -black		
						Clay -silty, brown		
						Silt -tan, moist		
						Clay -mottled brown		
						-highly plastic		
						-stiff to firm		
						-gypsum inclusions to 17'		
				10				
				20				
				30		grey		
				40				
				50		Glacial Till		
				60		-silty, sandy, gravelly		
						-tan, medium dense to soft		
						-wet to saturated		
						-cobbley and/or bouldery		
						-dense to very dense at 51'		
						-slight seepage at 56'		
						-medium dense below 56'		
						Notes:		
						1. Auger refusal at 59'.		
						2. Installed sealed standpipe at 47'.		
						Bottom 3' of standpipe slotted.		
						3. Water level at 29.5' from grade		
						on March 16/88.		

DYREGROV & BURGESS

BOREHOLE LOG

PROJECT

South End Water Pollution Control Centre

LOGGED/DWN.	SDG	CKD.	NCB	DATE OF INVEST.	29/02/88	JOB NO.	88528	HOLE NO.	2
				SOIL DESCRIPTION			SOIL SAMPLE		
				DATUM			CONDITION	TYPE	PENETRATION RESISTANCE
				SURFACE ELEVATION 763.06'					
W _p - □	w - ○	w _L - △		DEPTH (FT)	SOIL SYMBOL				
10	20	30	40	50	60				
				0	SS	TOPSOIL			
						Clay - silty -brown			
						Silt -tan -moist to wet			
						Clay -mottled brown -highly plastic -stiff to firm			
				10					
				20		-- grey			
				30					
				40					
				50					
				60					
						Glacial Till			
						-silty, sandy, gravelly -tan, soft to medium dense -wet to saturated -dense to very dense at 49' -cobbly and bouldery below 52' -medium dense below 59'			
						Notes:			
						1. Auger refusal at 67'. 2. Water level at 38' from grade in about 5 minutes.			

$$\begin{aligned} qu &= 2290 \text{ psf} \\ \gamma_w &= 113.3 \text{ pcf} \\ pp &= 4150 \text{ psf} \\ Tv &> 2000 \text{ psf} \end{aligned}$$

$$\begin{aligned} qu &= 1275 \text{ psf} \\ \gamma_w &= 105.6 \text{ pcf} \\ pp &= 1850 \text{ psf} \\ Tv &= 905 \text{ psf} \end{aligned}$$

DYREGROV & BURGESS

BOREHOLE LOG

PROJECT

South End Water Pollution Control Centre

LOGGED/DWN.	SDG	CKD.	NCB	DATE OF INVEST.	29/02/88	JOB NO.	88528	HOLE NO.	3
WATER CONTENT				DEPTH (FT)	SOIL SYMBOL	SOIL DESCRIPTION		SOIL SAMPLE	
W _p - □	W-O	W _L -△	PERCENT %			DATUM	SURFACE ELEVATION	CONDITION	TYPE
10	20	30	40	50	60		763.27'		PENETRATION RESISTANCE
Q	/	/	10	0	SS	Topsoil Clay - silty, brown			
						Silt - tan - moist, firm			
				10		Clay - mottled brown - highly plastic - stiff to firm		U	qu=1595psf $\gamma_w=106.7\text{pcf}$ pp=2880psf Tv=1660psf
				20		-- grey			
				30					
				40					
				50		Glacial Till - silty, sandy, gravelly - tan, soft - dense to very dense at 52' - bouldery below 54' - medium dense below 56'			qu=2115psf $\delta_w=110.5\text{pcf}$ pp=2200psf Tv=1320psf
				60		Notes: 1. Auger refusal at 63'. 2. Water level at 47' from grade in about 5 minutes.			

DYREGROV & BURGESS

BOREHOLE LOG

PROJECT

South End Water Pollution Control Centre

LOGGED/DWN.	SDG	CKD.	NCB	DATE OF INVEST.	1/03/88	JOB NO.	88528	HOLE NO.	4	
				SOIL SYMBOL	SOIL DESCRIPTION			DRILL TYPE		
WATER CONTENT			DEPTH		DATUM	SURFACE ELEVATION	764.18'	CONDITION	TYPE	PENETRATION RESISTANCE
W _p - □	W - O	W _L - △	PERCENT %	(FT)						
10	20	30	40	50	60					
				0	X	Fill -clay, trace gravel				
						Clay -black				
						Clay -silty, brown				
						Silt -tan, clayey, moist				
						Clay -mottled brown				
						-highly plastic				
						-stiff to firm				
				10		— grey		U		
				20						
				30						
				40						
				50		Glacial Till				
				60		-silty, sandy, gravelly				
						-tan, medium dense				
						-6" thick clay seams to 49'				
						-dense to very dense at 52'				
						-bouldery below 51'				
						-slight seepage upon drilling to .53'				
						Notes:				
						1. Auger refusal at 62.5'				
						Water level at 44' from grade in about 5 minutes				

DYREGROV & BURGESS**BOREHOLE LOG**

PROJECT

South End WAtter Pollution Control Centre

LOGGED/DWN.	SDG	CXO.	NCB	DATE OF INVEST.	1/03/88	JOB NO.	88528	HOLE NO.	5
				SOIL DESCRIPTION			SOIL SAMPLE		
				DATUM			CONDITION	TYPE	PENETRATION RESISTANCE
				SURFACE ELEVATION 763.35'					
Wp - □	w - ○	WL - △	PERCENT %	DEPTH (FT)	SOIL SYMBOL				
10	20	30	40	50	60				
				0	X	Fill -clay -trace gravel -organic clay			
				10		Silt -tan, moist, trace sand Clay -mottled brown -highly plastic -stiff to firm		U	
				20		-- grey		U	
				30					
				40					
				50		Glacial Till -silty, sandy gravelly -tan, soft to medium dense -dense at 52' -very dense and bouldery at 53' -slight seepage at 56' -medium dense below 57'			
				60		Notes: 1. Auger refusal at 63.5'. 2. Water level at 42' upon completion of drilling.			

DYREGROV & BURGESS

BOREHOLE LOG

PROJECT

South End Water Pollution Control Centre

LOGGED/DWN.	SDG	CKD.	NCR	DATE OF INVEST.	1/03/88	JOB NO.	88528	HOLE NO.	6	
WATER CONTENT				DEPTH (FT)	SOIL DESCRIPTION			SOIL SAMPLE		DRILL TYPE 18" Auger
W _p - □	W - O	W _L - Δ.	PERCENT %		DATUM	SURFACE ELEVATION	762.06'	CONDITION	TYPE	
10	20	30	40	50	60					OTHER TESTS
				0	X	Fill - clay, some gravel				
				10		Clay - mottled brown - highly plastic - stiff to firm				
				20		grey	U			qu=3500psf $\gamma_w=112.8\text{pcf}$ pp=3640psf Tv=1870psf
				30			U			qu=1700psf $\gamma_w=103.4\text{pcf}$ pp=2300psf Tv=1240psf
				40		Glacial Till - silty, sandy , gravelly - tan, soft - wet to saturated - medium dense at 51' dense and bouldery at 52' - slight seepage upon drilling to 54' - medium dense below 55'				
				50						
				60						
Notes:										
1. Auger refusal at 63'. 2. Water level at 50' from grade upon completion of drill.										

Plate 8

DYREGROV & BURGESS

BOREHOLE LOG

PROJECT

South End Water Pollution Control Centre

LOGGED/DWN.	SDG	CXD.	NCR	DATE OF INVEST.	1/03/88	JOB NO.	88528	HOLE NO.	7
WATER CONTENT				DEPTH (FT)	SOIL DESCRIPTION			SOIL SAMPLE	
W _p - □	W - O	W _L - Δ.	PERCENT %		DATUM	SURFACE ELEVATION	CONDITION	TYPE	PENETRATION RESISTANCE
10	20	30	40	50	60	762.90'			
				0	X	Fill -clay, some gravel, cobbly			
				10		Clay -black			
						Clay - silty, brown			
						Silt tan, moist			
						Clay - mottled brown			
						-highly plastic			
						-stiff to firm			
				20					
				30		-- grey			
				40					
				50		Glacial Till			
						- silty, sandy, gravelly			
						-tan, soft to medium dense			
						-bouldery			
						-very sandy at 53'			
						-dense at 53'			
						-seepage at 53'			
						-medium dense below 54'			
				60		Notes:			
						1. Auger refusal at 66' on possible bedrock.			
						2. Water level at 40' from grade upon completion of drilling.			

DYREGROV & BURGESS

BOREHOLE LOG

PROJECT

South End Water Pollution Control Centre

DYREGROV & BURGESS

BOREHOLE LOG

PROJECT

South End Water Pollution Control Centre

LOGGED/DWN.	SDG	CKD.	NCB	DATE OF INVEST.	2/03/88	JOB NO.	88528	HOLE NO.	9
WATER CONTENT				DEPTH (FT)	SOIL DESCRIPTION			DRILL TYPE	
W _p - □	w - ○	w _L - △	PERCENT %		DATUM	SAMPLE	CONDITION	TYPE	PENETRATION RESISTANCE
10	20	30	40	50	60	SURFACE ELEVATION 763.38'			
				0	X	Fill -clay, silt, trace gravel			
						Clay -black			
						Clay -silty -brown			
						Silt -tan, moist			
						Clay -mottled brown -highly plastic -stiff to firm			
				10		-- grey		U	
				20					
				30					
				40					
				50		Glacial Till -silty, sandy, gravelly -tan, clayey to 48' -saturated, soft, cobbly -slight seepage at 54' -bouldery below 56' dense from 56 to 58' -medium dense below 58'			
				60		Notes: 1. Auger refusal at 64.5' in broken bedrock. 2. Water level at 43 and hole open to 44' upon completion.			

DYREGROV & BURGESS

BOREHOLE LOG

PROJECT

South End Water Pollution Control Centre

LOGGED/DWN.	SDG	CKD.	NCB	DATE OF INVEST.	8/03/88	JOB NO.	88528	HOLE NO.	10	
WATER CONTENT				DEPTH (FT)	SOIL DESCRIPTION			SOIL SAMPLE		DRILL TYPE
W _P - □	W - O	W _L - Δ.	PERCENT %		DATUM	SURFACE ELEVATION 762.94'	CONDITION	TYPE	PENETRATION RESISTANCE	18" Auger
10	20	30	40	50	60					OTHER TESTS
				0	X	Fill -gravel, some clay				
				10		Silt -tan, moist				
				20		Clay -mottled brown -highly plastic -stiff to firm				
				30		grey				qu=2595psf $\gamma_w=108.7\text{pcf}$ pp=3500psf Tv=1650psf
				40						
				50		Glacial Till -silty, sandy, gravelly -tan, saturated, soft -seepage at 52' -dense from 55 to 58' -medium dense below 58'				qu=2750psf $\gamma_w=108.9\text{pcf}$ pp=2240psf Tv=950psf
				60		Notes: 1. Auger refusal at 66.5' on probable bedrock. 2. Water at 39' from grade upon completion of drilling.				

DYREGROV & BURGESS

BOREHOLE LOG

PROJECT

South End Water Pollution Control Centre

LOGGED/DWN:	SDG	CKD.	NCB	DATE OF INVEST.	8/03/88	JOB NO.	88528	HOLE NO. 11
WATER CONTENT			DEPTH (FT)	SOIL DESCRIPTION		SOIL SAMPLE		DRILL TYPE 18" Auger
W _p - □	W - O	W _L - Δ.		DATUM	SURFACE ELEVATION	CONDITION	TYPE	
PERCENT %	10 20 30 40 50 60							
			0	Topsoil -black Clay -mottled brown -highly plastic -stiff to firm -gypsum inclusions				
			10					
			20					
			30	--grey				
			40					
			50	Glacial Till -silty, sandy, gravelly -tan, saturated, soft -seepage at 52' -bouldery at 54' -dense from 54 to 56'				
			60	Notes: 1. Auger refusal at 64' on probable bedrock. 2. Hole open to 45' upon completion of drilling. 3. Placed sealed standpipe at 55'.				

qu=3435psf
 $\gamma_w=110.0\text{pcf}$
pp=4880psf
T_v=1940psf

qu=1835psf
 $\gamma_w=113.2\text{pcf}$
pp=1760psf
T_v=1000psf

Notes:(Cont'd)
4. Water level at 30' from grade on March 16/88.

DYREGROV & BURGESS

BOREHOLE LOG

PROJECT

South End Water Pollution Control Centre

LOGGED/DWN.	SDG	CKD.	NCB	DATE OF INVEST.	8/03/88	JOB NO.	88528	HOLE NO.	12	
WATER CONTENT			DEPTH (FT)	SOIL SYMBOL	SOIL DESCRIPTION			SOIL SAMPLE		DRILL TYPE 18" Auger
W _p	-□-	W _O	W _L	-△-	DATUM	CONDITION	TYPE	PENETRATION RESISTANCE		
10	20	30	40	50	60	SURFACE ELEVATION 762.59'				
					0	Fill -gravel, clay, concrete				
					10	Clay -mottled brown -highly plastic -stiff to firm	U		qu=1180psf $\gamma_w=106.9\text{pcf}$ pp=3200psf Tv=1640psf	
					20					
					30	grey	U		qu=2390psf $\gamma_w=110.5\text{pcf}$ pp=3080psf Tv=1570psf	
					40					
					50	Glacial Till -silty, sandy, gravelly -tan, soft to medium dense -dense at 55' -very sandy at 56' -seepage at 56'				
					60	Notes: 1. Auger refusal at 66' on probable bedrock. 2. Hole open to 48' upon completion				

**GEOTECHNICAL REPORT
PROPOSED DISINFECTION BUILDING
SOUTH END WATER POLLUTION CONTROL CENTRE
CITY OF WINNIPEG**

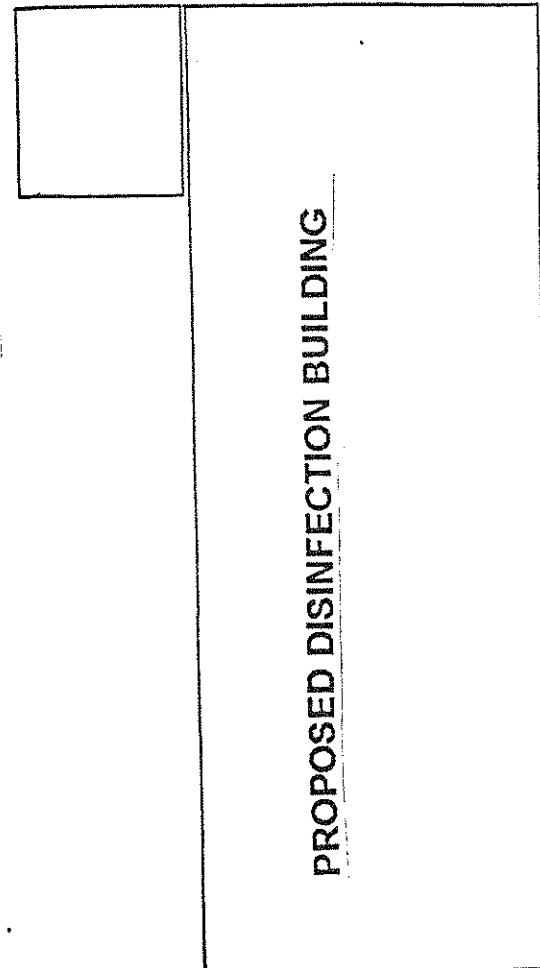
**PREPARED FOR
REID CROWTHER & PARTNERS LTD.**

February 1998

Project 981754

O
TH 1

CHLORINE CONTACT CHAMBER



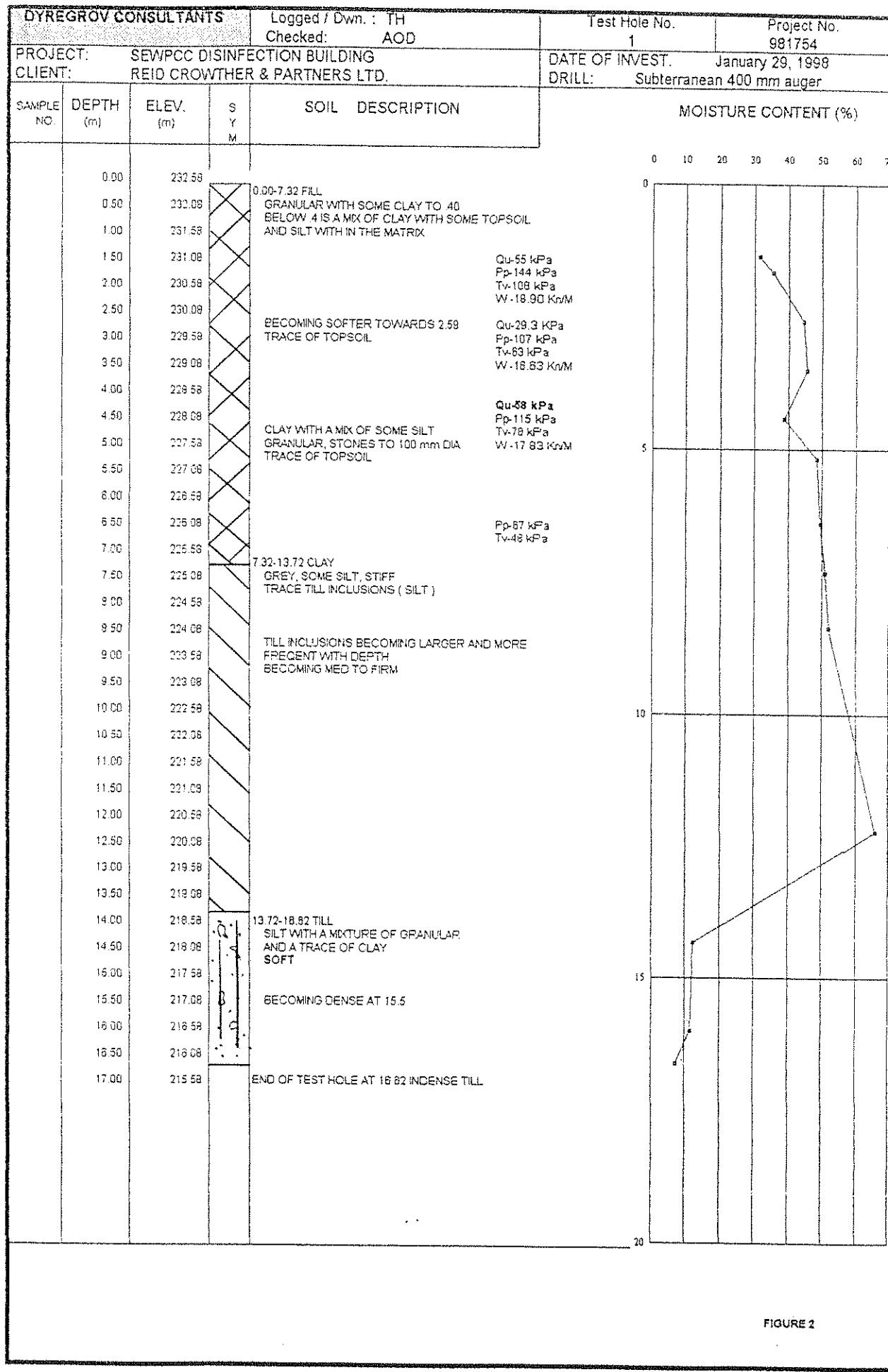
O
TH 2

O
TH 3

Y N

DYREGROW CONSULTANTS
CONSULTING GEOTECHNICAL ENGINEERS

TEST HOLE LOCATION PLAN
PROPOSED DISINFECTION BUILDING
SEWPCC



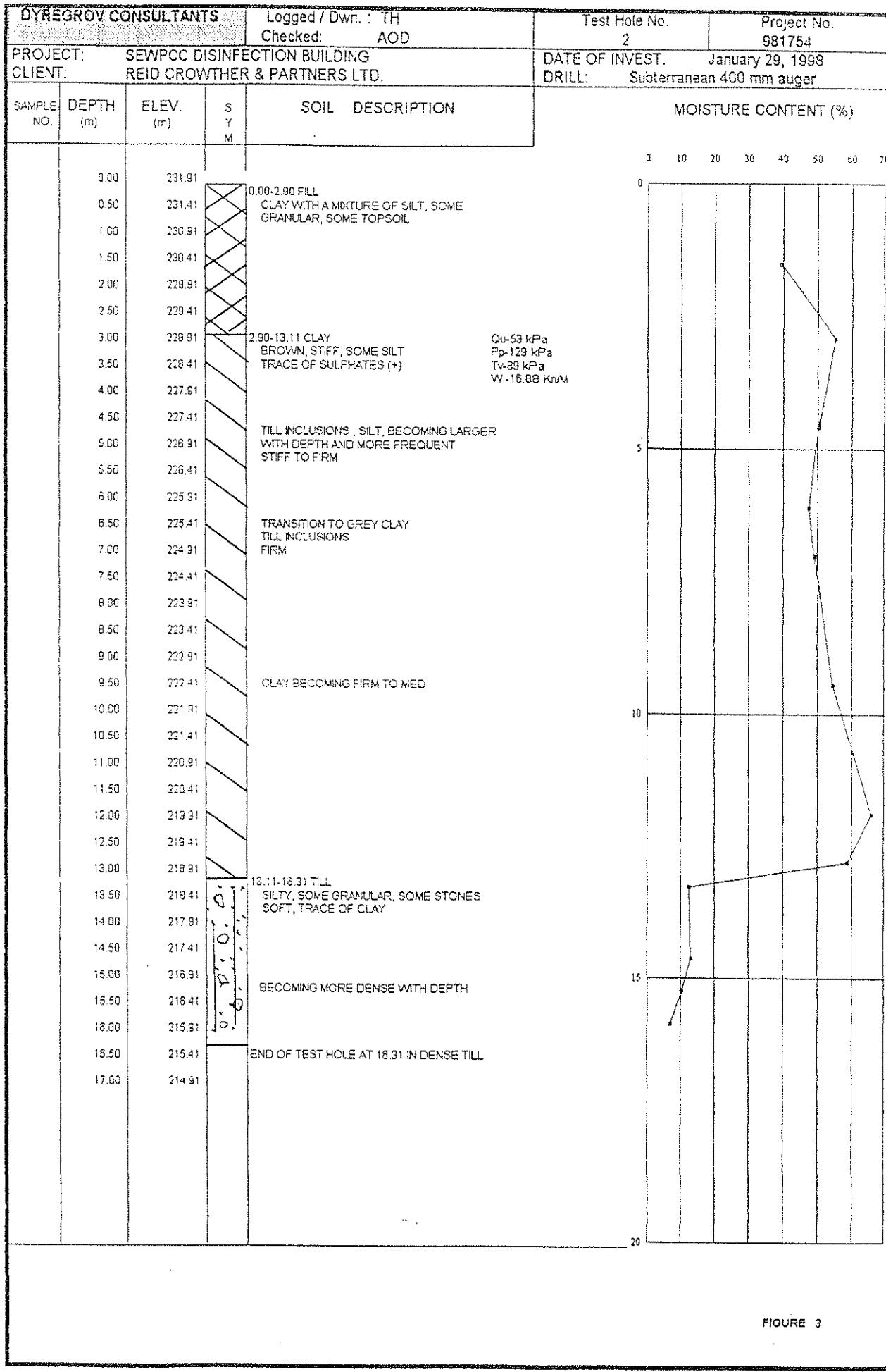
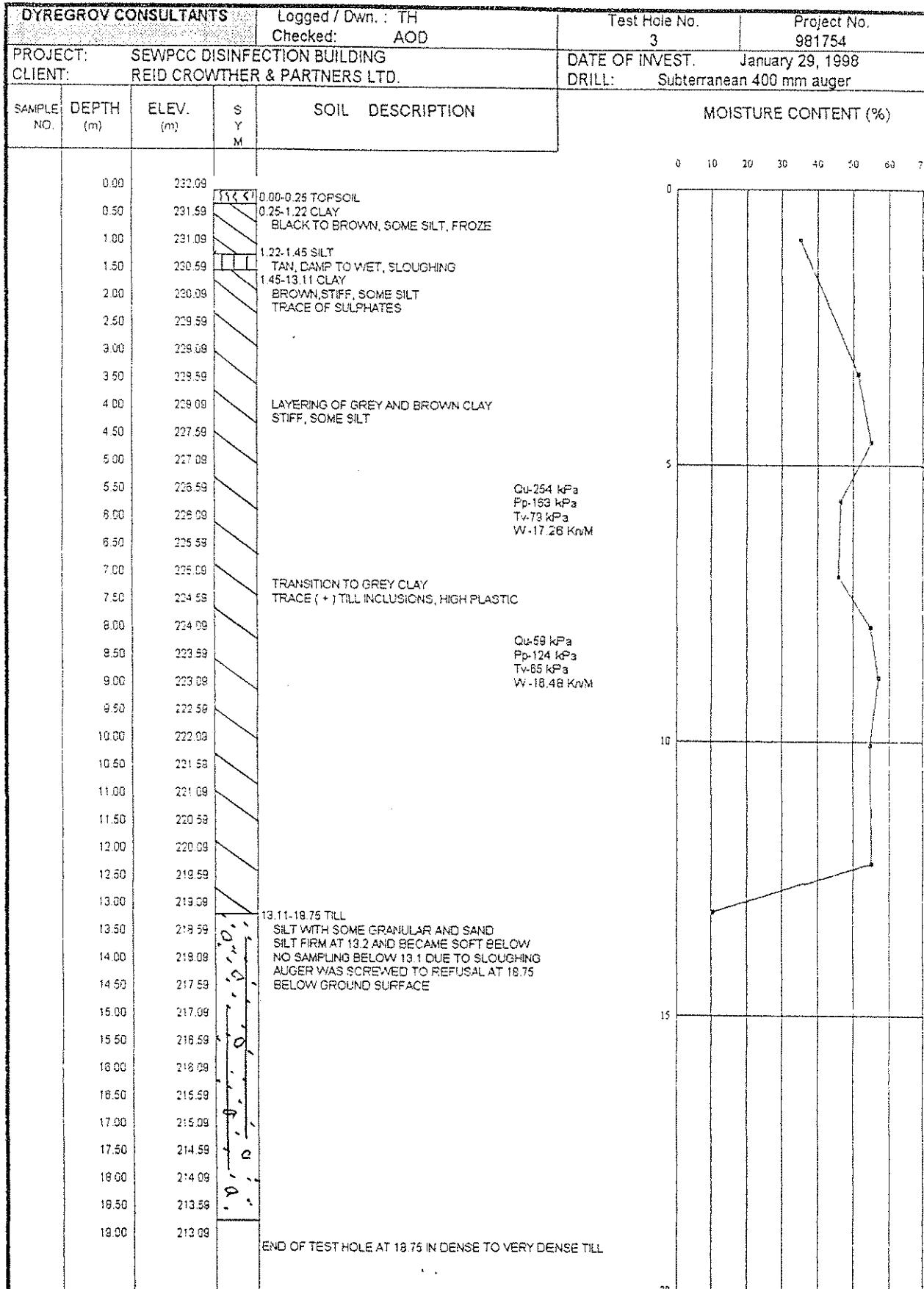
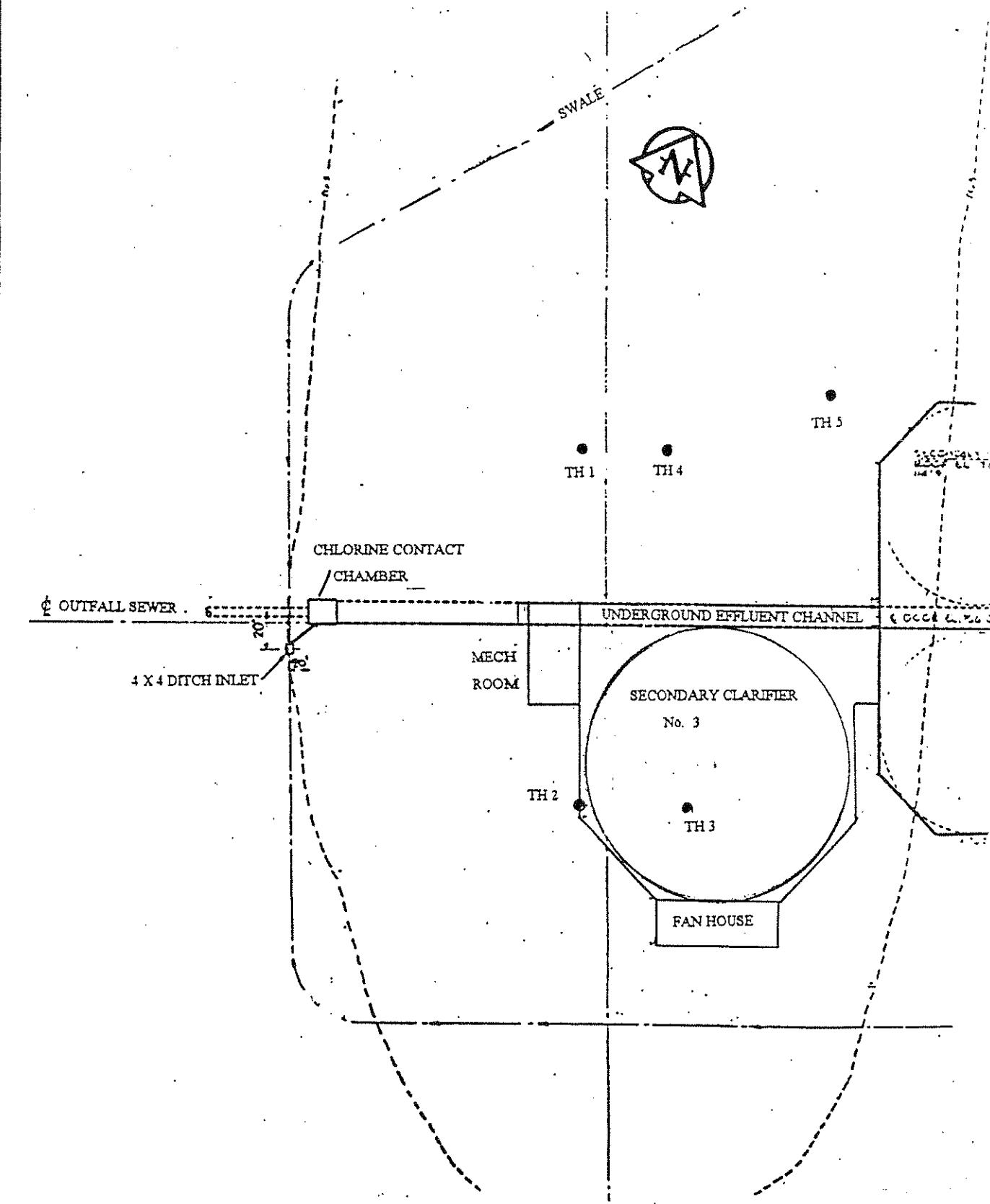


FIGURE 3



NOTE: WATER AT 7.5 BELOW SURFACE AFTER 20 MINUTES

FIGURE 4



DYREGROV CONSULTANTS
CONSULTING GEOTECHNICAL ENGINEERS

CONTROL CENTRE
SITE PLAN